Intended for Dynegy Midwest Generation, LLC 10901 Baldwin Road Baldwin, IL 62217

Date February 18, 2025

Project No. 1940110241-005

CORRECTIVE ACTION GROUNDWATER MONITORING PLAN

BALDWIN POWER PLANT, FLY ASH POND SYSTEM, IEPA ID NO. W1578510001-01, W1578510001-02, AND W1578510001-03



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Project name Project no. Recipient Document type Revision Date Baldwin Power Plant Fly Ash Pond System 1940110241-005 Dynegy Midwest Generation, LLC Corrective Action Groundwater Monitoring Plan DRAFT February 18, 2025

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ACRONYMS AND ABBREVIATIONS

35 I.A.C.	Title 35 of the Illinois Administrative Code
40 C.F.R.	Title 40 of the Code of Federal Regulations
ASD	Alternative Source Demonstration
BPP	Baldwin Power Plant
CCR	coal combustion residuals
COC	constituent of concern
CSM	conceptual site model
DMG	Dynegy Midwest Generation, LLC
E001	Event 1
FAPS	Fly Ash Pond System
GMP	Groundwater Monitoring Plan
gpm	gallons per minute
GWMS	groundwater management system
GWPS	groundwater protection standard
ID	identification
IEPA	Illinois Environmental Protection Agency
IPCB	Illinois Pollution Control Board
No.	Number
PMP	Potential migration pathway
QA/QC	quality assurance/quality control
Ramboll	Ramboll Americas Engineering Solutions, Inc.
RL	reporting limit
SI	surface impoundment
StAP	Statistical Analysis Plan
UA	uppermost aquifer
UU	Upper unit
USEPA	United States Environmental Protection Agency

1. INTRODUCTION

1.1 Overview

In accordance with requirements of Title 35 of the Illinois Administrative Code (35 I.A.C.) § 845: Standards for the Disposal of Coal Combustion Residuals in Surface Impoundments, Ramboll Americas Engineering Solutions, Inc. (Ramboll) has prepared this Corrective Action Groundwater Monitoring Plan (GMP) on behalf of Baldwin Power Plant (BPP), operated by Dynegy Midwest Generation, LLC. (DMG). This GMP will apply specifically to the coal combustion residuals (CCR) Multi-Unit referred to as the Fly Ash Pond System (FAPS; CCR unit identification [ID] number [No.] 605 and National Inventory of Dams [NID] No. IL50723). The FAPS consists of three CCR SIs including the Old East Fly Ash Pond System (Illinois Environmental Protection Agency [IEPA] ID No. W1578510001-01), the East Fly Ash Pond (IEPA ID No. W1578510001-02), and the West Fly Ash Pond (IEPA ID No. W1578510001-03). The FAPS is a closed, unlined CCR Multi-Unit that was previously used to manage CCR and non-CCR waste streams at the BPP. This Corrective Action GMP includes content requirements specific to 35 I.A.C. § 845.630 (*Groundwater Monitoring System*), 35 I.A.C. § 845.640 (*Groundwater Sampling and Analysis*), 35 I.A.C. § 845.650 (*Groundwater Monitoring Program*), and 35 I.A.C. § 845.680 (*Implementation of the Corrective Action Plan*) for the FAPS at the BPP.

A checklist in **Table 1-1** provides references to sections, tables, and figures within this document that meet the specific requirements of 35 I.A.C. § 845.630, 35 I.A.C. § 845.640, 35 I.A.C. § 845.650, and 35 I.A.C. § 845.680.

This Corrective Action GMP will be included as Appendix B.1 to the Construction Permit Application for the BPP FAPS. DMG completed significant source control efforts in 2020 as part of final closure of the FAPS [1]. The final closure was performed in accordance with the Closure and Post-Closure Care Plan [2] that was developed in accordance with Title 40 of the Code of Federal Regulations (40 C.F.R.) § 257 and submitted to IEPA for review. IEPA found "...that the plan...represent an appropriate means by which to close the Baldwin Fly Ash Pond System which is comprised of the East Fly Ash Pond, the Old East Fly Ash Pond and the West Fly Ash Pond" [3].

The Corrective Action Plan proposes source control with a groundwater management system (GMS) as the remedy for the FAPS. As described in the Corrective Action Plan, the proposed remedy meets the performance standards of 35 I.A.C. § 845.670(d) and addresses all current and potential future releases from the FAPS. Likewise, this Corrective Action GMP establishes how data will be collected, documented, and evaluated to assess remedy effectiveness for all currently documented and potential future releases from the FAPS¹ per the process outlined in **Figure 1-1**.

Adaptive site management strategies are an integral part of corrective action groundwater monitoring. The adaptive site management approach consistent with National Research Council, Interstate Technology & Regulatory Council and United States Environmental Protection Agency (USEPA) methodologies will allow timely incorporation of new site information throughout corrective action to ensure the achievement of the groundwater protection standard (GWPS). The adaptive site management approach expedites progress toward meeting the GWPS while acknowledging uncertainties, such as the persistence of current groundwater flow directions and

¹ The presence of exceedances at the waste boundary will continue to be evaluated under the Operating permit GMP previously submitted to IEPA [8].

potential related changes in geochemical conditions. The structured decision-making process proposed in this Corrective Action GMP includes specific metrics used to evaluate remedy progress, criteria which would trigger adaptive management evaluation, and options for those management actions.

1.2 Site Location and Background

The BPP is located in southwest Illinois in Randolph and St. Clair Counties. The Randolph County portion of the BPP is located within Sections 2, 3, 4, 9, 10, 11, 14, 15, and 16 of Township 4 South and Range 7 West. The St. Clair County portion of the property is located within Sections 33, 34, and 35 of Township 3 South and Range 7 West. The FAPS is approximately one-half mile west-northwest of the Village of Baldwin (**Figure 1-2**).

The BPP property is bordered to the west by the Kaskaskia River; to the east by Baldwin Road, farmland, and strip-mining areas; to the southeast by the village of Baldwin; to the south by the Illinois Central Gulf railroad tracks, scattered residences, and State Route 154; and to the north by farmland. The St. Clair/Randolph County Line crosses east-west at approximately the midpoint of Baldwin Lake (*i.e.*, Cooling Pond). **Figure 1-2** shows the location of the BPP; **Figure 1-3** is a site map showing the location of the FAPS (a 35 I.A.C. § 845 regulated CCR Unit and the subject of this GMP), Bottom Ash Pond (BAP), Secondary Pond, Tertiary Pond, and Cooling Pond. Information regarding the BAP, Secondary Pond, Tertiary Pond, and Cooling Pond is solely for background information, as this GMP applies specifically to the FAPS CCR unit, which will hereinafter be referred to as the Site.

1.3 Conceptual Site Model

Significant site investigation has been completed at the BPP to characterize the geology, hydrogeology, and groundwater quality. Based on the extensive investigation and monitoring, the FAPS has been well characterized, as detailed in the Hydrogeologic Site Characterization Report [4] (HCR), Nature and Extent Report [5] and HCR Revision 1 that was provided for the adjacent BAP [6], which were prepared to comply with the requirements specified in 35 I.A.C. § 845.620. These documents expand upon the Hydrogeologic Monitoring Plan [7] and the conceptual site model as presented below.

In addition to CCR, materials at the BPP have been categorized into two hydrostratigraphic units at the FAPS based on stratigraphic relationships, geologic composition, and common hydrogeologic properties. The units, listed from surface downward, are summarized as follows:

- **Upper Unit (UU):** Predominantly clay with some silt and minor sand, silt layers, and occasional sand lenses. Includes the lithologic layers identified as the Cahokia Alluvium, Peoria Loess, Equality Formation, and Vandalia Till Member. This unit is composed of unlithified natural geologic materials and extends from the upper saturated materials to the bedrock. Thin sand seams and the interface (contact) between the UU and bedrock have been identified as potential migration pathways (PMPs). No continuous sand seams were observed within or immediately adjacent to the FAPS; however, the sand seams may act as a PMP due to relatively higher hydraulic conductivities. The acronym UU and the materials it contains is synonymous with Upper Groundwater Unit used in previous documents.
- **Bedrock Unit:** This unit is considered the Uppermost Aquifer (UA) and is composed of interbedded shale and limestone bedrock, which underlies and is continuous across the entire Site.

Groundwater flow in the UA (**Figure 1-4**) is generally to the west and southwest across the Site toward the Kaskaskia River. Groundwater flow in bedrock is toward the northwest in the east and central areas of the BAP, and southwest to northwest on the east area of the FAPS until groundwater reaches the bedrock valley feature underlying the Secondary and Tertiary Ponds west of the BAP and FAPS, at which point the flow direction veers towards this bedrock surface low.

Immediately upgradient and downgradient of the BPP property boundaries, both the shallow glacial deposits and the shallow bedrock have served as a source of water supply. The shallow unlithified deposits off-site have yielded water through intermittent, discontinuous sand lenses and, in the bedrock, through fractured sandstone and limestone. However, within the area of the Site, investigations have indicated only thin and intermittent sand lenses are present within predominantly clay deposits; thus, the unlithified materials do not represent a continuous aquifer unit. Based on these details, the Bedrock Unit was designated as the UA in the *Supplemental Hydrogeologic Site Characterization and Groundwater Monitoring Plan* [8], consistent with the USEPA definition in 40 C.F.R. § 257.53.

The shallow bedrock is the only water-bearing unit that is continuous across the Site. Shallow sandstone and creviced limestone may yield small supplies in some areas, but water quality becomes poorer (*i.e.*, highly mineralized) with increasing depth. The Pennsylvanian and Mississippian rocks generally have low porosities and permeabilities, are not a reliable source of groundwater, and the quality varies considerably [9]. Therefore, the lower limit of the UA is the depth at which either the groundwater is mineralized to a point that it is no longer a useable water source, or the secondary porosities do not yield a sufficient volume of groundwater to produce a useable water supply.

1.4 Groundwater Quality

Groundwater monitoring in accordance with the proposed Operating GMP and sampling methodologies provided in the operating permit application for groundwater compliance at the FAPS began in the second quarter of 2023 [10]. The proposed compliance monitoring wells yield groundwater samples that represent the quality of downgradient groundwater at the CCR boundary (as required in 35 I.A.C. § 845.630(a)(2)).

The Event 1 (E001) quarterly groundwater monitoring event was completed on May 23, 2023. In accordance with 35 I.A.C. § 845.610(b)(3)(C), and the statistical analysis plan submitted with the operating permit application (Appendix A of the Groundwater Monitoring Plan Revision 1) constituent concentrations observed at compliance wells were evaluated for compliance with the GWPSs summarized in 35 I.A.C. § 845.600 to determine exceedances² of the GWPS. The following GWPS exceedances were determined at compliance groundwater monitoring wells [11]:

- Boron at wells MW-150 and MW-391
- Sulfate at well MW-150

² Throughout this document, "exceedance" or "exceedances" is intended to refer only to potential exceedances of proposed applicable background statistics or Groundwater Protection Standards (GWPSs) as described in the proposed groundwater monitoring program, which was submitted to the IEPA on October 25, 2021, as part of Dynegy Midwest Generation, LLC's operating permit application for the Baldwin Fly Ash Pond System. That operating permit application, including the proposed groundwater monitoring program, remains under review by the IEPA and therefore Dynegy Midwest Generation, LLC has not identified any actual exceedances.

Subsequent compliance sampling events (following E001) were also evaluated for exceedances of the GWPS as described in 35 I.A.C. § 845.600. Additional exceedances identified during the subsequent events [12, 13, 14, 15, 16] consist of the following:

- Boron at well MW-152
- Fluoride at well MW-384
- pH at wells MW-253 and MW-350
- Sulfate at wells MW-252, MW-253R, and MW-366

Pursuant to 35 I.A.C. § 845.650(e), an Alternative Source Demonstration (ASD) was completed for the pH exceedance [17] detected at MW-253 during the Quarter 3, 2023 event and received concurrence in a letter from the IEPA dated March 7, 2024 [18]. The ASD identified contamination of the groundwater by grout used in construction of the monitoring well as the alternative source for the GWPS exceedance. Consequently, a work plan to address this contamination via well abandonment and replacement was submitted to the IEPA on March 14, 2024 [19]. Similar conditions were also observed historically in background well MW-306 and compliance well MW-350 during Quarter 1, 2024, and these wells were also proposed for abandonment in the work plan. The IEPA provided written concurrence with the work plan on April 9, 2024 [20] and the wells were subsequently abandoned and replaced in early May of 2024.

During evaluation of results from groundwater sampling and Alternative Source Demonstrations, inconsistencies in concentrations and water level measurements at background well MW-358 and compliance well MW-391 were identified. Well construction at each location was inspected using a downhole camera and identified that the well casings were compromised. A plan to abandon and replace the wells was submitted to the IEPA [21] and approved in a letter/email dated September 17, 2024. The monitoring wells were replaced in October 2024, and following installation, MW-391R has been dry during monitoring events. This is consistent with the original wells at this location, MW-387 and MW-391, prior to its suspected failure in 2018. This is an indication that the bedrock at this location does not yield recoverable amounts of water and there are no potential exceedances of the GWPS at this location.

In accordance with 35 I.A.C. § 845.660, a Corrective Measures Assessment was developed to address current and potential future GWPS exceedances originating from the FAPS, excluding the pH exceedances at wells MW-253 and MW-350 as addressed in the ASD and associated work plan, and was submitted to IEPA on April 24, 2024 [22]. The selected remedy will meet the performance standards of 35 I.A.C. § 845.670(d) and once implemented and completed, the selected remedy presented in the Corrective Action Plan will attain the GWPSs.

1.5 Supplemental Site Investigation

Additional investigations were conducted in 2024 in accordance with 35 I.A.C. § 845.650 to further assess the nature, degree, and extent of boron groundwater impacts downgradient of the FAPS.

A total of four monitoring wells were installed off-site, south of the FAPS, in two phases to further delineate the extent of boron concentrations above the 35 I.A.C. § 845 GWPS. Soil samples were collected from the unconsolidated material at each location and submitted for full mineral analysis, clay mineral analysis, cation exchange capacity, metals, and loss on ignition. Three wells were

installed across PMPs within the UU in May of 2024 (MW-195, MW-196, and MW-197). After two rounds of sampling, an additional monitoring well was installed in October of 2024 (MW-198).

The Supplemental Site Investigation fully delineated the boron impacts to groundwater downgradient of the FAPS. Boron has migrated laterally to the southwest through PMPs within the UU; however, the lateral migration does not extend greater than 300 feet off-site and is limited by the creek adjacent to the BPP [23].

Sulfate concentrations above the GWPS were first detected at MW253R in July 2024 following installation of the well in May 2024. The monitoring well was installed to replace MW-253 which was impacted by grout contamination. Concentrations measured in groundwater shortly after well installation and development are often not representative of long-term stabilized concentrations, specifically in low permeability units like the UU. Additional samples collected in August and October, 2024 confirmed the elevated concentrations of sulfate and evaluation of the nature and extent of these concentrations is ongoing but is expected to be limited in extent.

2. CORRECTIVE ACTION GROUNDWATER MONITORING PLAN

This Corrective Action GMP is being provided to propose a groundwater monitoring program specific to the FAPS that will comply with 35 I.A.C. § 845.680. The Corrective Action GMP will monitor and evaluate groundwater quality specifically to document the effectiveness of the corrective action remedy. The groundwater monitoring program will include sampling and analysis procedures that are consistent and that provide an accurate representation of groundwater quality.

2.1 Corrective Action Groundwater Monitoring Program and Parameters

2.1.1 35 I.A.C. § 845 Corrective Action Groundwater Monitoring

The proposed 35 I.A.C. § 845 corrective action monitoring well network will consist of 11 wells to document the effectiveness of the corrective action remedy and ultimately demonstrate compliance with GWPSs (**Figure 2-1**). The wells included in the corrective action monitoring well network include select compliance monitoring wells from the Operating GMP network (*e.g.*, those with previously reported exceedances of the GWPS) (**Section 1.4**) and monitoring wells installed during the Supplemental Site Investigation (**Section 1.5**).

As appropriate to meet the corrective action monitoring objectives and evaluate the effectiveness of the corrective action remedy (as described in **Section 3**), the corrective action monitoring program involves assigning each well to a monitoring category or purpose (**Table 2-1**). These monitoring categories include:

- Inside Plume- wells located at the CCR boundary with GWPS exceedances.
- Plume Definition wells located along the lateral or vertical boundary of the plume.

A summary of the well locations and associated purpose as it relates to the above categories is presented in **Table 2-1** and **Figure 2-1**. Monitoring well depths and construction details are listed in **Table 2-2** and boring logs and monitoring well construction forms are provided in **Appendix A**. Groundwater samples will be collected and analyzed for the laboratory and field parameters in **Table 2-3**. Laboratory parameters include major ions for evaluating groundwater chemistry and constituents of concern (COCs) (*i.e.*, reported exceedances in accordance with the Operating GMP) the Corrective Action is intended to address. Sampling to evaluate corrective action effectiveness will begin the quarter after the corrective action remedy is implemented and commissioned.

2.2 Sampling Schedule

All wells in the 35 I.A.C. § 845 corrective action GMP network, as presented in **Table 2-1**, will be sampled quarterly to provide a complete picture of corrective action effectiveness. Groundwater elevations will be determined at the time of sample collection from each well. Sampling will end in accordance with 35 I.A.C. § 845.680(c), when compliance with the GWPS has been demonstrated "at all points within the plume of contamination that lies beyond the waste boundary [...] for a period of three consecutive years" (details in **Section 3.3**).

Consistent with 35 I.A.C. § 845.650(b)(4), quarterly sampling may be reduced to a semiannual frequency with IEPA approval after completion of five years of monitoring. A request for reduced sampling frequency will include a demonstration that corrective action monitoring effectiveness will not be compromised; sufficient data has been collected to evaluate ongoing remedy effectiveness; and existing data show trends consistent with anticipated remedy performance (details in **Section 3.1**).

2.3 Groundwater Sample Collection

Groundwater samples will be collected and analyzed in accordance with the Multi-Site Sampling and Analysis Plan [24]. Groundwater sampling procedures have been developed and the collection of groundwater samples is being implemented to meet the requirements of 35 I.A.C. § 845.640. In addition to groundwater well samples, quality assurance samples will be collected as described in **Section 2.5** (**Table 2-3**).

2.4 Laboratory Analysis

Laboratory analysis will be performed consistent with the requirements of 35 I.A.C. § 845.640(j) by a state-certified laboratory using methods approved by IEPA and USEPA. Laboratory methods may be modified based on laboratory equipment availability or procedures, but the Reporting Limit (RL) for all parameters analyzed, regardless of method, will be lower than the applicable groundwater quality standard [24]. Concentrations lower than the RL will be reported as less than the RL.

2.5 Quality Assurance Program

Consistent with the requirements of 35 I.A.C. § 845.640(a)(5), the sampling and analysis program includes procedures and techniques for quality assurance/quality control (QA/QC). Additional quality assurance samples to be collected will include the following:

- Field duplicates will be collected at a frequency of one per group of ten or fewer investigative water samples.
- One equipment blank sample will be collected and analyzed for each day of sampling. If dedicated sampling equipment is used, then equipment blank samples will not be collected.
- The duplicate and equipment blank quality assurance samples will be supplemented by the laboratory QA/QC program, which typically includes:
 - Regular generation of instrument calibration curves to assure instrument reliability
 - Laboratory control samples and/or quality control check standards that have been spiked, and analyses to monitor the performance of the analytical method
 - Matrix spike/matrix spike duplicate analyses to determine percent recoveries and relative percent differences for each of the parameters detected
 - Analysis of replicate samples to check the precision of the instrumentation and/or methodology employed for all analytical methods
 - Analysis of method blanks to assure that the system is free of contamination

Water quality meters used to measure pH and turbidity will be calibrated according to manufacturer's specifications. At a minimum, it is recommended that calibration of pH occur daily prior to sampling and checked for accuracy at the end of each day. Unusual or suspect pH

measurements during sampling events will be flagged, evaluated, and additional calibration may be performed throughout the sampling events. Turbidity meters will be checked daily, prior to and following sampling. Unusual measurements or erratic meter performance will be flagged and evaluated for overall effects on the data prior to reporting.

2.6 Groundwater Monitoring Well Maintenance Plan

Consistent with the requirements of 35 I.A.C. § 845.630(e)(2), maintenance will be performed according to the Multi-Site Quality Assurance Project Plan [25] as needed to assure that the monitoring wells provide representative groundwater samples. Monitoring wells will be inspected during each groundwater sampling event; inspections will consist of the following:

- Visual inspection, clearing of vegetation, replacement of markers, and painting of protective casings as needed to assure that monitoring wells are clearly marked and accessible
- Visual inspection and repair or replacement of well aprons as needed to assure that they are intact, drain water away from the well, and have not heaved
- Visual inspection and repair or replacement of protective casings as needed to assure that they are undamaged, and that locks are present and functional
- Checks to assure that well caps are intact and vented, unless in flood-prone areas in which case caps will not be vented
- Routine measurement of monitoring well depths to determine the degree of siltation within the wells. Wells will be redeveloped as needed to remove siltation from the screened interval if it impedes flow of water into the well
- Checks to assure that wells are clear of internal obstructions, and flow freely

If wells are damaged or become otherwise inoperable, they will be replaced by wells screened at the same elevation and as close to the original well as possible (ideally within 10 feet) and notification will be provided to IEPA. If a replacement well cannot be installed within approximately 10 feet of the original well location, notification will be sent to IEPA and a monitoring well will be installed as close as possible to the original monitoring well and given a new well identification number. Any well replacement activities will also be documented in the Annual Groundwater Monitoring and Corrective Action Report.

2.7 Statistical Analysis

A Multi-Site Statistical Analysis Plan (StAP) has been developed to describe the statistical procedures that will be used to evaluate the groundwater results [26].

2.8 Data Reporting

Groundwater monitoring and analysis completed in accordance with 35 I.A.C. § 845 under an approved monitoring program will be reported to IEPA annually by January 31 as required by I.A.C. § 845.550, for data collected the preceding year. The Annual Groundwater Monitoring and Corrective Action Report will include the status of the groundwater monitoring and Corrective Action Plan for the FAPS in addition to other requirements detailed in 35 I.A.C. § 845.610(e).

2.9 Compliance with Applicable Groundwater Protection Standards

As provided in 35 I.A.C. § 845.680(c)(2), corrective action is considered complete when compliance with the GWPS has been achieved by demonstrating that concentration of

constituents listed in 35 I.A.C. § 845.600 have not exceeded the GWPSs for a period of three consecutive years, using the statistical procedures and performance standards in 35 I.A.C. § 845.640(f) and (g).

Attainment of GWPSs and conclusion of corrective action monitoring is discussed below in **Section 3.3**.

If a new exceedance is determined during monitoring under the Operating GMP, the Corrective Action groundwater monitoring program will be evaluated for monitoring of additional locations and/or constituents using the adaptive site management methods presented herein.

3. EFFECTIVENESS OF THE CORRECTIVE ACTION REMEDY

The methods for evaluating the effectiveness of the corrective action remedy described in this section are based on the following guidance documents:

- "Methods for Evaluating the Attainment of Cleanup Standards Volume 2: Ground Water," USEPA, Office of Policy, Planning, and Evaluation, 1992 [27].
- "Groundwater Remedy Completion Strategy: Moving Forward with the End in Mind," Office of Solid Waste and Emergency Response, 2014 [28].
- "Adaptive Site Management A Framework for Implementing Adaptive Management at Contaminated Sediment Superfund Sites," USEPA, Office of Superfund Remediation and Technology Innovation, 2022 [29].
- "Environmental Cleanup Best Management Practices: Effective Use of the Project Life Cycle Conceptual Site Model," USEPA, Office of Solid Waste and Emergency Response, 2011 [30].

Evaluation of corrective action remedy effectiveness will occur in three phases (**Figure 3-1**): remedy progress evaluation, stability evaluation, and attainment evaluation [31].

- 1. Remedy progress evaluation occurs after implementation of corrective actions to assesses if the remedy is functioning as anticipated.
- 2. The stability evaluation, which occurs after groundwater management system has been concluded and a re-equilibration period has elapsed, assesses if a new post-groundwater management system steady state in the groundwater has been reached.
- 3. Attainment evaluation occurs after a new steady state has been achieved and assesses if COC concentrations are below the GWPS.

COCs are parameters with exceedances of the GWPS to be addressed by the Corrective Action Plan. Corrective action monitoring at BPP FAPS includes the following COC parameters:

• Boron, fluoride, and sulfate

The effectiveness of the remedy at each phase is evaluated using performance metrics designed to assess the goals of that phase. Performance metrics answer questions designed to evaluate multiple aspects of remedy effectiveness with the ultimate goal of holistically guiding management decisions [32]. These metrics may be evaluated using qualitative (subject to expert judgement) or quantitative (numerical outcomes) methods.

This section details the goals and performance metrics of each phase of remedy evaluation. Within each phase, the well groups described in **Section 2.1** have distinct applicable metrics and/or potential management actions consistent with the role of that well group within the corrective action monitoring framework. The remedy evaluation metrics documented here are specific to wells within the Corrective Action monitoring program.

3.1 Remedy Progress Evaluation

The goal of remedy process evaluation is to determine if a groundwater remedy is on track to achieve cleanup standards within the proposed time frame and to inform adaptive management decisions if performance metrics are not achieved. Evaluation of remedy progress includes evaluating the response of COCs in individual monitoring wells and in the plume as a whole.

Remedy progress is evaluated using performance metrics as described below. **Table 3-1** details the questions used to assess remedy progress and metrics which would trigger additional evaluation of adaptive site management options. **Figure 3-2** presents an outline of the decision-making process regarding adaptive management actions (the first step of which is assessing remedy progress per **Table 3-1**).

Documentation of remedy progress metrics will be provided in the Annual Groundwater Monitoring and Corrective Action Report (**Section 2.8**) beginning after the second year of data collection: a minimum of eight data points is required to complete meaningful statistical analysis required for evaluation of the remedy progress metrics, which will be available after two years of quarterly sampling. Per USEPA guidance [32], a thorough review of corrective action progress and remedy effectiveness will be conducted every five years. A Five-Year Annual Groundwater Monitoring and Corrective Action Report will evaluate the comprehensive data set and, if triggered by the results of the remedy progress evaluation metrics (**Table 3-1**), evaluate whether adaptive management actions are needed (**Figure 3-2**). The five-year time frame allows adaptive management decisions to be based on robust data sufficient to complete meaningful statistical analysis while remaining responsive to changing site conditions [32]. The remedy progress evaluation metrics and triggers for additional evaluation are described below.

3.1.1 Comparison to Groundwater Protection Standard

The Inside Plume wells in this monitoring plan were defined based on exceedances of the GWPS. The question posed to evaluate whether exceedances of the GWPS occur, and associated method of evaluation is (**Table 3-1**):

• Are COC concentrations greater than the GWPS? – Compare data points or summary statistics to site-specific GWPS values.

COC concentrations below the GWPS in Inside Plume wells may indicate that remedial actions are approaching completion and that moving to the next phase of remedy effectiveness evaluation may be warranted (see **Section 3.2**). Persistence of COC concentrations above the GWPS in Plume Definition wells may indicate that the plume is no longer properly delineated. Therefore, the trigger criterion for further evaluation is a central tendency measure of the last eight data points exceeding the GWPS.

3.1.2 Agreement with Groundwater Model

A groundwater flow and transport model³ was used to compare the anticipated time to reach the GWPS for the different corrective actions considered at the FAPS.

The question posed to evaluate agreement of corrective action remedy progress with the groundwater model results is provided in **Table 3-1** and summarized below:

 Are concentrations of COCs at individual wells consistent with modeling expectations? – Evaluate if the observed results track with the predicted results in general direction and magnitude using expert professional judgement.

Only Inside Plume and Plume Definition wells included in the flow and transport model are evaluated according to this metric. Trigger criteria for additional adaptive site management

³ The Groundwater Modeling Technical Memorandum is included as an attachment to the Corrective Actions Alternative Assessment presented as part of the Corrective Action Plan.

evaluation include monitoring results failing to follow the general magnitude and direction of groundwater model results at one or more locations. It is acceptable to conclude that no further adaptive site management evaluation is triggered if future observations do not precisely match modeled results on an individual well basis if the direction of remedy progress is adequate.

3.1.3 Trend Analysis

Evaluation of COC trends in wells both within and outside of the plume is a major component of remedy progress evaluations [31, 32]. Decreasing COC concentrations within the groundwater plume provides critical support for remedy effectiveness evaluations. Changing concentrations in wells defining the plume may indicate unanticipated plume migration or a need for better plume definition. Both short-term and long-term trends are important to evaluate remedy performance [31]. All trend analyses are performed in accordance with the Corrective Action StAP and the USEPA Unified Guidance for groundwater statistics [33].

The questions posed to evaluate if COC concentrations are decreasing in Inside Plume wells and the associated methods for evaluation are provided in **Table 3-1** and summarized as follows:

 Are average plume COC concentrations decreasing? – Evaluate trend based on quarterly average of COC concentrations of Inside Plume wells, both for the last eight sampling events and since corrective action was initiated.

The questions posed to evaluate if COC concentrations are changing in Inside Plume wells and Plume Definition wells and the associated methods for evaluation are provided in **Table 3-1** and summarized below:

Are concentrations of COCs at individual wells changing? – Evaluate trend of COC concentrations, both for the last eight sampling events and since corrective action was initiated.

The goal of the corrective action is to reduce COC concentrations in the groundwater. Therefore, trigger criteria have been established for the three types of corrective action monitoring wells as follows:

- Inside Plume well triggers for adaptive site management evaluation are based on no decreasing trend in COC concentrations (short-term or long-term).
- Plume Definition well triggers are based on increasing COC concentrations, which may indicate improper delineation of the plume. Therefore, the trigger criterion for adaptive site management evaluation at Plume Definition wells is increasing short- or long-term trend.

3.1.4 Adaptive Management Actions

The goal of adaptive management actions is to understand why performance metrics are not met and, if the remedy is found to be unsuccessful in meeting remediation goals, drive supplemental corrective actions or, in extreme cases, re-evaluation of remedy selection. This section describes in greater detail the steps in the flow chart presented in **Figure 3-2** (adapted from Figure 2 in [32]).

As the remedy progress evaluation metrics are evaluated annually, failure to meet the metrics (as described in **Table 3-1**) leads to further action. If the data available at the time of the Five-Year Review are anticipated to be inadequate for determining the need for adaptive site

management actions, additional data may be collected before the Five-Year Review including collecting samples from additional wells or measuring additional parameters.

If the remedy progress is not found to be adequate during the Five-Year Review, the most critical question is whether or not the remedy is likely to achieve the GWPS in a reasonable time frame. This may be evaluated using methods such as regression analysis or analysis of groundwater flow with respect to operation of the GWMS. If the remedy progress is not judged to be adequate but the remedy is likely to achieve the GWPS in a reasonable time frame, the CSM or the groundwater model may require updating to reflect evolving field conditions⁴. Additional data collected may also suggest ways to optimize the monitoring network or performance metrics [32].

If the remedy does not appear likely to achieve the GWPS in a reasonable time frame, it may be due to changing hydrogeochemical dynamics within the plume or an additional source of COCs not accounted for in the CSM. If available data suggests either occurrence, the Five-Year Review will describe additional activities planned to investigate if the existing remedy is still a viable option for attaining the GWPS. If the remedy is still viable, an update to the CSM and groundwater model is likely required and will be conducted after additional investigation is completed.

If the remedy does not appear likely to achieve the GWPS in a reasonable time frame, there is no alternative source of COCs not accounted for in the CSM, and the plume is appropriately delineated; or if the investigation into the hydrogeochemical changes or alternative source of COCs determines that the remedial action is no longer solely viable as a corrective action, an evaluation of additional remedial actions will be initiated.

If the remedy progress evaluation metrics indicate that concentrations across the monitoring network are below the GWPS (and the GWMS system has ceased operation; see **Section 3.1.5**), the remedy progress phase may be considered complete, and the monitoring program may move to the Stability Evaluation phase (see **Section 3.2**).

3.1.5 Concluding operation of the GMS

Groundwater modeling used to support design of the GMS (Appendix B of the CAAA-SIR) [34] estimates the selected remedy of source control with the GMS will attain the GWPS in greater than 100 years. The GMS is intended to reduce the accumulation of hydraulic head beneath the FAPS cover system which reduces the potential for liquids from the FAPS to mix with groundwater and migrate past the limits of the FAPS towards the BPP southern property boundary. Source control with GMS was the most effective remedy at reducing predicted concentrations of CCR derived constituents in groundwater and minimizing the footprint of impacted groundwater. The GMS operation will only be ceased when concentrations of COCs at on-site wells adjacent to the system do not exceed the GWPS. Additional considerations such as trends in COC concentrations, analysis of groundwater flow, or seasonal variability may also influence the decision of whether to cease operating the GWMS.

A period of equilibration and rebound is typical when discontinuing groundwater management system operations and caution should be used when interpreting short-term changes in COC

⁴ As stated in Section 1.4.1 of the Corrective Action Plan: "Estimated timelines for GWMS and times to reach GWPS will be periodically reviewed and updated based on observed corrective action performance via an adaptive site management strategy."

concentrations [27]. The groundwater flow and transport model may be revised to estimate the potential for rebound to occur. A "slack period" of one year (or more, based on modeling results, if applicable) will be allowed to elapse after conclusion of groundwater management system operations before stability and GWPS attainment are evaluated.

3.2 Stability Evaluation

Evaluation of groundwater stability reflects the idea that implementation of a remedy will, by necessity, cause changes to the physical and chemical environment of the groundwater. In order to evaluate ultimate effectiveness of the remedy, it is critical to evaluate if a new stable equilibrium has been reached after groundwater management system has been discontinued. Stability is achieved when groundwater elevations are stable (accounting for seasonal variability), average COC concentrations are stable across all wells, and COC concentrations are stable at each well. If groundwater management operations have been stopped, a slack period of at least one year is recommended before evaluating stability [31].

Trends in groundwater elevation and COC concentrations at each plume well will be evaluated using the most recent eight data points (*i.e.*, two years of data when sampling quarterly) according to methods presented in the Corrective Action StAP. This metric is met for a plume well when there is no statistically significant trend in groundwater elevation or COC concentrations.

Plume COC concentrations will be evaluated for trend using the most recent eight data points, with the average concentration across plume wells per sampling event considered as one data point, according to methods presented in the Corrective Action StAP. This metric is met when there is no statistically significant trend in average COC concentrations.

3.3 Attainment Evaluation and Conclusion of Corrective Action Monitoring

The ultimate goal of groundwater corrective action is to attain compliance with the GWPS for each COC in Inside Plume wells. After stability has been achieved per the metrics discussed in **Section 3.2**, attainment evaluation will begin. Per 35 I.A.C. § 845.680(c), corrective action is considered complete when compliance with the GWPS has been demonstrated "at all points within the plume of contamination that lies beyond the waste boundary [...] for a period of three consecutive years". Attainment of the GWPS will be evaluated in accordance with the StAP. Corrective action monitoring is considered complete for the site when COCs in the corrective action monitoring well network do not exceed the GWPS for three years.

4. REFERENCES

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Table 1-1. 35 I.A.C. § 845 Requirements Checklist

Corrective Action Groundwater Monitoring Plan Baldwin Power Plant Fly Ash Pond System Baldwin, IL

35 I.A.C. § 845 Reference	35 I.A.C. § 845 Components	Location of Information in Corrective Action GMP		
845.630	Groundwater Monitoring Systems			
845.630(a)(2)	Potential contaminant pathways must be monitored.	ΝΑ		
845.630(a) 845.630(b) 845.630(c)	At least two upgradient wells and four downgradient wells (min. 1 and 3, but requires additional documentation)	Section 2.1 Figure 1-4		
845.630(a) 845.630(b) 845.630(c)	Downgradient Well Density	Figure 1-4		
845.630(a)(2)	Downgradient wells at waste boundary	Figure 1-4		
845.640	Groundwater Sampling and Analysis Requirements			
845.640(a)	Consistent sampling and analysis procedures	Section 2 Tables 2-3 and 2-4		
845.640(b)	Methods are appropriate	Section 2 Tables 2-3 and 2-4		
845.640(c)	Groundwater elevations must be measured in each well prior to purging, each time groundwater is sampled.	Section 2.2		
845.640 (d)(e)(f)(g)(h)	Establishment of background and application of statistical methods	Section 2.7 Appendix A		
845.640(i)	Analyze total recoverable metals	Table 2-3		
845.640(j)	Analyze groundwater samples using a certified laboratory	Section 2.4		
845.650	Groundwater Monitoring Program			
845.650(a)	Must include monitoring for all constituents with a groundwater protection standard in Section 845.600(a), calcium, and turbidity	Section 2.1 Table 2-3		
845.650(b)(c)	Groundwater Monitoring Frequency	Section 2.2		
845.650(d)(e)	Exceedances of the groundwater protection standard	Sections 2.9 and 3.1.1		
845.650(b)(2) and (3)	Staff gauge/ piezometer to monitor head in impoundment	NA		
NA	Staff gauge/ piezometer to monitor head of neighboring surface water body	NA		
845.680	Implementation of the Corrective Action Plan			
845.680(a)(1)(a)	Establish and implement a corrective action groundwater monitoring program that meets requirements of 845.650	Sections 2.1 and 3 Tables 2-1 and 3-1 Figure 2-1		
845.680(a)(1)(b)	Document the effectiveness of the corrective action remedy	Section 3		
845.680(a)(1)(c)	Demonstrate compliance with the groundwater protection standard under Subsection [845.680] (c)	Sections 2.9 and 3		
845.680(c)(1)	Demonstrate compliance with the groundwater protection standards established by 845.600 has been achieved at all points within the plume of contamination that lies beyond the waste boundary	Section 3.3		
B45.680(c)(2) Demonstrate that concentrations of constituents listed in standards for a period of three consecutive years using statistical procedures and performance standards in 845.640(f) and (g)		Sections 3.3 and 3.4		

	[O: EGP 12/05/24; C: CJC 01/17/25]

Notes:

GMP = Groundwater Monitoring Plan NA = Not Applicable



Table 2-1. Summary of Monitoring Well Locations and Purpose

Corrective Action Groundwater Monitoring Plan Baldwin Power Plant Fly Ash Pond System Baldwin, IL

Corrective Action Monitoring Well System Monitored Well ID Unit **Inside Plume Plume Definition** MW-150 PMP Х MW-152 PMP Х MW-252 PMP Х MW-253R PMP Х MW-350R UA X MW-352 UA Х MW-366 UA Х MW-384 UA Х Х OW-257 PMP PZ-174 PMP Х PZ-176 PMP Х

[O: EGP 1/14/25; C: CJC 1/17/25; U: AOC 02/06/25]

Notes:

PMP = Potential Migration Pathway

UA = Uppermost Aquifer



Table 2-2. Monitoring Well Locations and Construction Details

Corrective Action Groundwater Monitoring Plan

Baldwin Power Plant

Fly Ash Pond System

Baldwin, IL

Location	HSU	Date Constructed	Top of PVC Elevation (ft)	Measuring Point Elevation (ft)	Measuring Point Description	Ground Elevation (ft)	Screen Top Depth (ft bgs)	Screen Bottom Depth (ft bgs)	Screen Top Elevation (ft)	Screen Bottom Elevation (ft)	Well Depth (ft bgs)	Bottom of Boring Elevation (ft)	Screen Length (ft)	Screen Diameter (inches)	Latitude (Decimal Degrees)	Longitude (Decimal Degrees)
MW-150	PMP	2010-09-01	396.76	396.93	Top of Casing	394.08	15	24.7	379.08	369.38	25.2	368.88	9.6	2	38.189408	-89.878474
MW-152	PMP	2010-09-01	424.94	425.11	Top of Casing	422.12	7.5	16.7	414.62	405.42	17.2	404.92	9.3	2	38.187576	-89.866771
MW-252	PMP	2010-09-01	424.94	425.11	Top of Casing	422.29	44.4	49	377.89	373.29	49.5	372.79	4.6	2	38.18757	-89.866752
MW-253R	PMP	2024-05-01	445.49	445.66	Top of Casing	442.65	29.5	34.5	413.15	408.15	35	407.65	5	2	38.185890	-89.860997
MW-350R	UA	2024-05-03	396.13	396.30	Top of Casing	394.13	42	47	352.13	347.13	47	347.13	5	2	38.189423	-89.878453
MW-352	UA	2010-09-01	424.76	424.93	Top of Casing	422.39	67.9	72.5	354.49	349.89	73	348.59	4.6	2	38.187560	-89.866736
MW-366	UA	2015-12-04	424.91	425.08	Top of Casing	422.51	42	52	380.51	370.51	52	368.21	10	2	38.192192	-89.872345
MW-384	UA	2015-12-18	458.70	458.87	Top of Casing	456.60	60.5	70.5	396.10	386.10	70.5	362.50	10	2	38.191789	-89.860699
OW-257	PMP	2013-08-01	430.94	431.11	Top of Casing	428.30	34	38.5	394.30	389.80	39.1	388.70	4.5	2	38.193873	-89.867461
PZ-174	PMP	2015-08-04	401.30	401.47	Top of Casing	399.07	14.5	24.5	384.57	374.57	24.5	374.37	10	2	38.189689	-89.877215
PZ-176	PMP	2015-08-06	405.72	405.89	Top of Casing	403.61	18.1	28.1	385.51	375.51	28.6	375.01	10	2	38.188573	-89.871629

Notes:

Notes: All elevation data are presented relative to the North American Vertical Datum 1988 (NAVD88), GEOID 12A bgs = below ground surface ft = foot or feet HSU = Hydrostratigraphic Unit PMP = Potential Migration Pathway UA = Uppermost Aquifer

[O: RAB 1/14/25; C: EGP 1/17/25; U: AOC 02/06/25]



Table 2-3. Sampling and Analysis Summary

Corrective Action Groundwater Monitoring Plan Baldwin Power Plant Fly Ash Pond System Baldwin, IL

Parameter	Analytical Method ¹	Number of Samples	Field Duplicates ²	Field Blanks ³	Equipment Blanks ³	MS/MSD ⁴	Total	Container Type	Minimum Volume ⁵	Preservation (Cool to 4 °C for all samples)	Sample Hold Time from Collection Date
Corrective Action Parameter(s) ⁶	-	-	-		-				-		
Boron	6020 ⁷	11	2	0	0	1	14	plastic	600 mL	HNO_3 to $pH<2$	6 months
Fluoride	9214 or EPA 300	11	2	0	0	1	14	plastic	300 mL	Cool to 6 °C	28 days
Sulfate	9036 or EPA 300	11	2	0	0	1	14	plastic	50 mL	Cool to 6 °C	28 days
norganic Parameters									-		
Alkalinity, bicarbonate	SM 2320 B	11	2	0	0	1	14	plastic	500 mL	Cool to 6 °C	14 days
Alkalinity, carbonate	SM 2320 B	11	2	0	0	1	14	plastic	500 mL	Cool to 6 °C	14 days
Calcium	6020 ⁷	11	2	0	0	1	14	plastic	600 mL	HNO_3 to $pH<2$	6 months
Chloride	9251 or EPA 300	11	2	0	0	1	14	plastic	100 mL	Cool to 6 °C	28 days
Magnesium	6020 ⁷	11	2	0	0	1	14	plastic	600 mL	HNO_3 to $pH<2$	6 months
Potassium	6020 ⁷	11	2	0	0	1	14	plastic	600 mL	HNO ₃ to pH<2	6 months
Sodium	6020 ⁷	11	2	0	0	1	14	plastic	600 mL	HNO ₃ to pH<2	6 months
Total Dissolved Solids	SM2530C	11	2	0	0	1	14	plastic	200 mL	Cool to 6 °C	7 days
ield Parameters					•					•	
pН	SM 4500-H+ B	11	NA	NA	NA	NA	11	flow-through cell	NA	none	immediately
Dissolved Oxygen ⁸	SM 4500-0/405.1	11	NA	NA	NA	NA	11	flow-through cell	NA	none	immediately
Temperature ⁸	SM 2550	11	NA	NA	NA	NA	11	flow-through cell	NA	none	immediately
Oxidation/Reduction Potential ⁸	SM 2580 B	11	NA	NA	NA	NA	11	flow-through cell	NA	none	immediately
Specific Conductance ⁸	SM 2510 B	11	NA	NA	NA	NA	11	flow-through cell	NA	none	immediately
Turbidity ⁹	SM 2130 B	11	NA	NA	NA	NA	11	flow-through cell or hand-held turbidity meter	NA	none	immediately

Notes:

¹ Analytical method numbers are from SW-846 unless otherwise indicated. Analytical methods may be updated with more recent versions as appropriate.

² Field duplicates will be collected at a frequency of one per group of 10 or fewer investigative water samples. Field duplicates will not be collected for radium analysis.

³ Field blanks will be collected at the discretion of the project manager; Equipment blanks will be collected at a rate of 1 per sampling event if non-dedicated equipment is used.

⁴ Matrix Spike/Matrix Spike Duplicate (MS/MSD) samples will be collected at a frequency of one per group of 20 or fewer investigative water samples per CCR unit/multi-unit. Additional volume to be determined by laboratory.

⁵ Sample volume is estimated and will be determined by the laboratory.

⁶ Determined by reported exceedances under the Operating Groundwater Monitoring Plan

⁷ Metals may be analyzed via ICP/ICPMS USEPA methods 6010 or 6020 depending on laboratory instrument availability.

⁸ Parameter collected for quality assurance and quality control for field sampling purposes only; not required to be collected or reported under 35 IAC § 845; collection of parameter may be discontinued without notification. ⁹ If turbidity exceeds 10 NTUs, a duplicate sample filtered through a 0.45 micron filter may be collected for metals analysis in addition to the unfiltered sample. Both samples would be submitted for analysis.

< = less than

^oC = degrees Celsius

 $HNO_3 = nitric acid$

mL = milliliter

NA = not applicable

NTU = nephelometric turbidity unit



Table 3-1. Adaptive Site Management Metrics and Trigger Criteria

Corrective Action Groundwater Monitoring Plan Baldwin Power Plant Fly Ash Pond System Baldwin, IL

QUESTION	Are COC concentrations greater than the GWPS?		Are concentrations of COCs at individual wells consistent with modeling expectations? ^a		Are the average COC concentrations decreasing?	Are concentrations of COCs at individual wells changing?	
EVALUATION^b	Compare data points or summary statistics to site-specific GWPS		Do the observed results track with the predicted results in general direction and magnitude? (Professional judgement)		Evaluate trend on quarterly average of well concentrations, both for last 8 data points and since corrective action initiated or closure completed	Evaluate trend of COCs at each well, both for last 8 data points and since corrective action initiated	Adaptive Site Management Outcome
Inside Plume	Central tendency concentration of last eight data points above the GWPS	D	Results inconsistent with model	HAN ONE OF	Neither trend decreasing	Neither trend decreasing	Evaluation ered ure 3-2)
Lateral/Vertical Plume Definition	Central tendency concentration of last eight data points above the GWPS	AN	Results inconsistent with model	AND MORE T	-	Either trend increasing	Additional Trigg (See Figu
NOTES						[O: AOC 07/22/24; C: CJC	12/05/24; U: AOC 02/06/

NOTES:

a. Only applies to wells included in the flow and transport model b. To be documented in Annual Monitoring and Corrective Action Reports

-- = No relevant trigger criteria

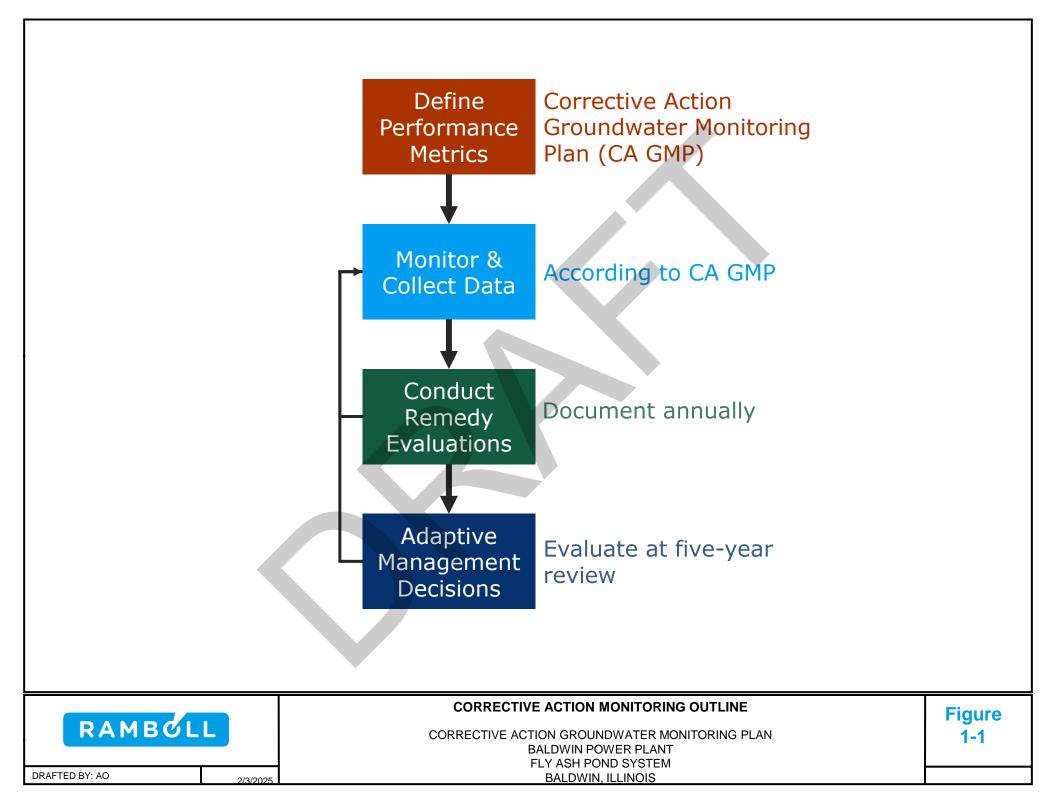
COC = constituent of concern

CSM = conceptual site model

GWPS = groundwater protection standard







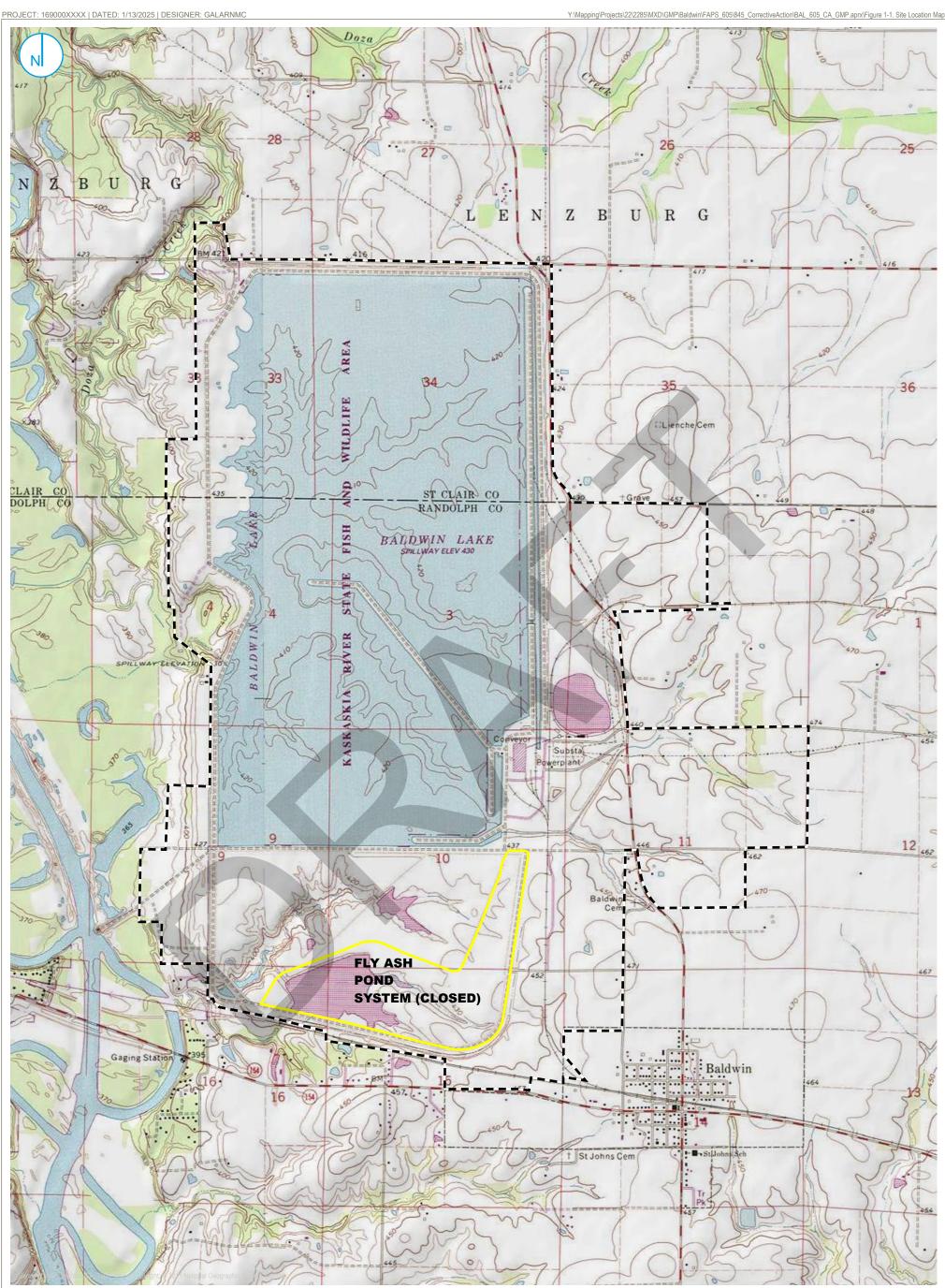


FIGURE 1-2

RAMBOLL AMERICAS ENGINEERING SOLUTIONS, INC.



CORRECTIVE ACTION GROUNDWATER MONITORING PLAN **FLY ASH POND SYSTEM** BALDWIN POWER PLANT BALDWIN, ILLINOIS

SITE LOCATION MAP



0 1,000 2,000 __ Feet L





800 I Feet

400

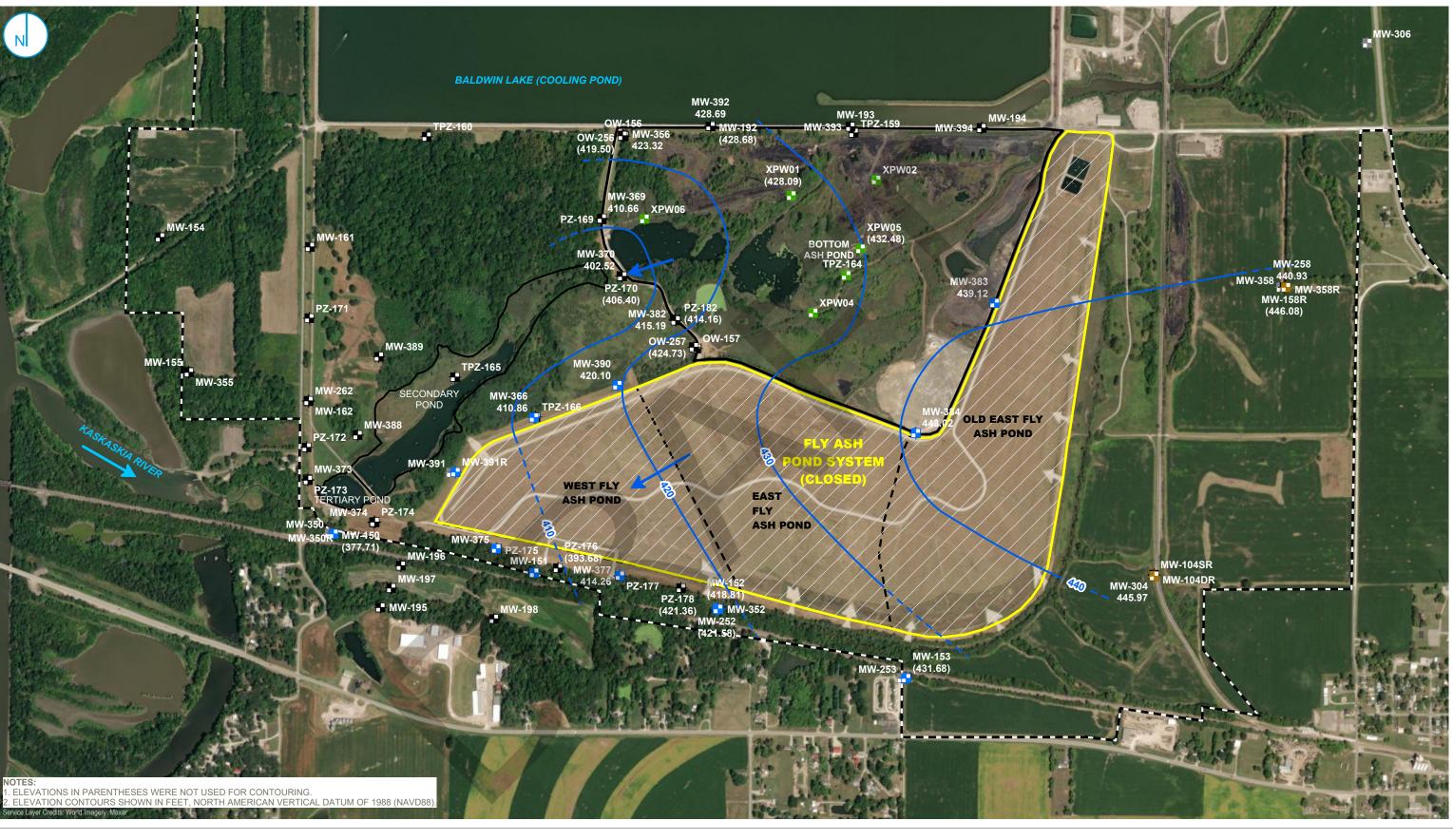
FIGURE 1-3

RAMBOLL AMERICAS ENGINEERING SOLUTIONS, INC.



SITE MAP

CORRECTIVE ACTION GROUNDWATER MONITORING PLAN FLY ASH POND SYSTEM BALDWIN POWER PLANT BALDWIN, ILLINOIS



- COMPLIANCE MONITORING WELL
- BACKGROUND MONITORING WELL
- HONITORING WELL
- PORE WATER WELL
- CLOSED MONITORING WELL
- CONTOUR (10-FT CONTOUR INTERVAL, NAVD88) INFERRED GROUNDWATER ELEVATION CONTOUR

GROUNDWATER ELEVATION

- → GROUNDWATER FLOW DIRECTION
- REGULATED UNIT (SUBJECT UNIT)

 SITE FEATURE

 CAPPED AREA

 DEODEETT(ROUNDAD)(

PROPERTY BOUNDARY

POTENTIOMETRIC SURFACE MAP NOVEMBER 10, 2024

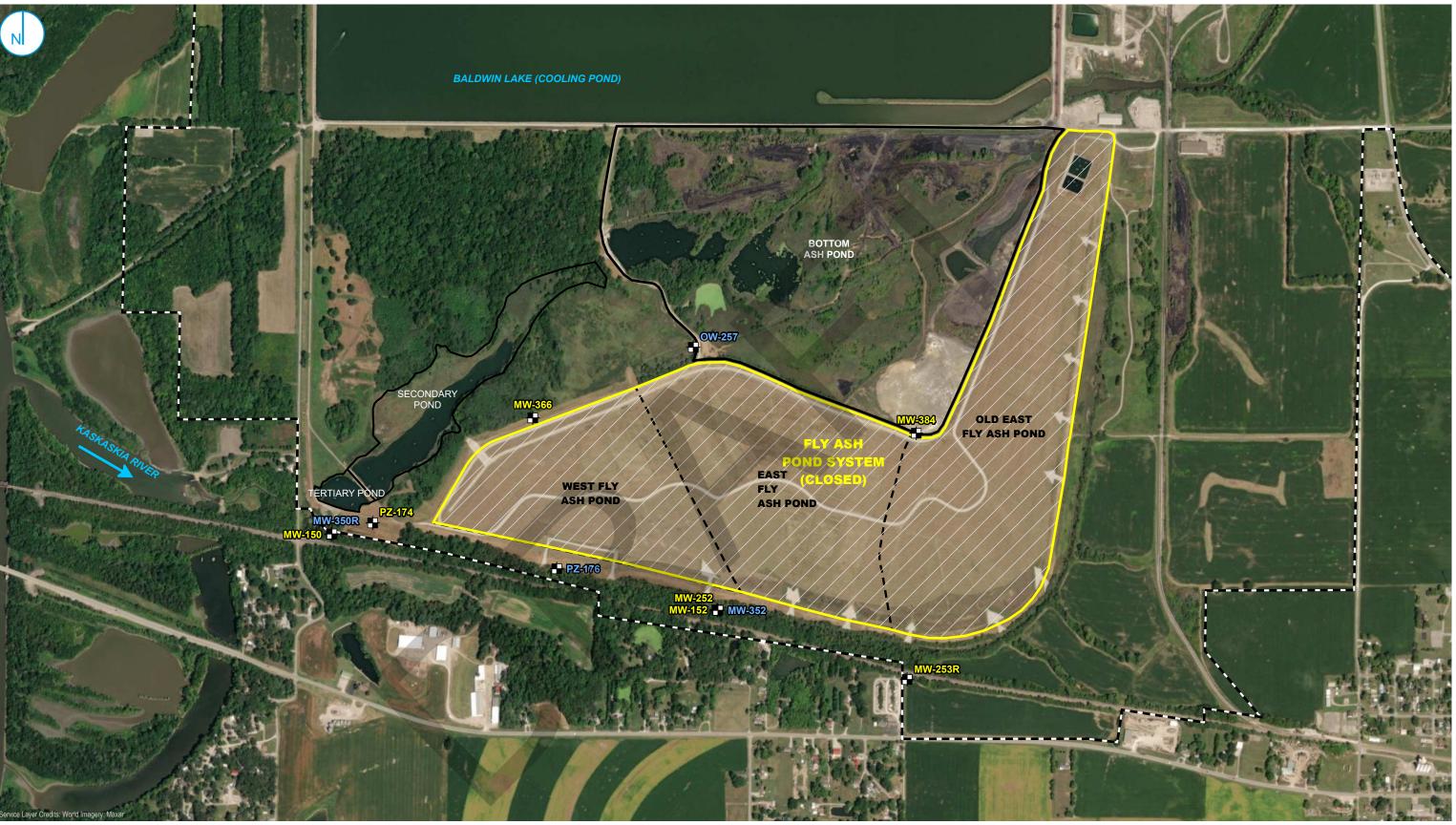
CORRECTIVE ACTION GROUNDWATER MONITORING PLAN FLY ASH POND SYSTEM BALDWIN POWER PLANT BALDWIN, ILLINOIS

400 800

FIGURE 1-4

RAMBOLL AMERICAS ENGINEERING SOLUTIONS, INC.









PROPOSED 35 I.A.C. § 845 CORRECTIVE ACTION MONITORING WELL LOCATION MAP

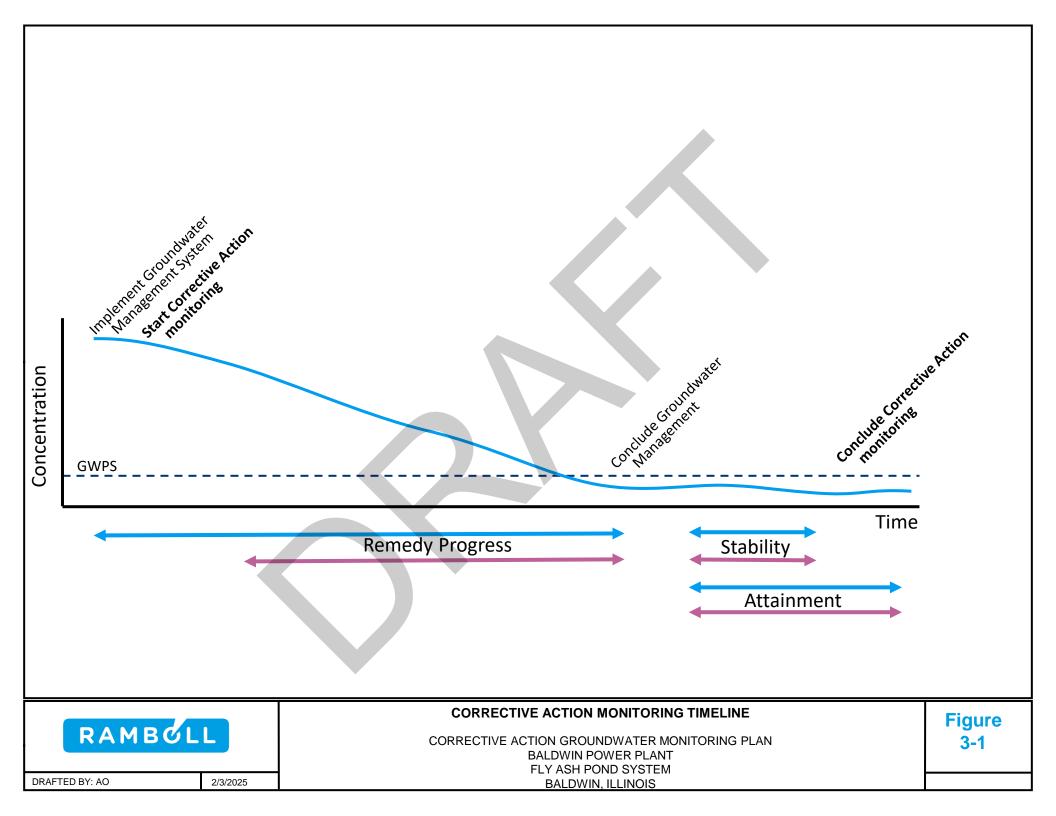


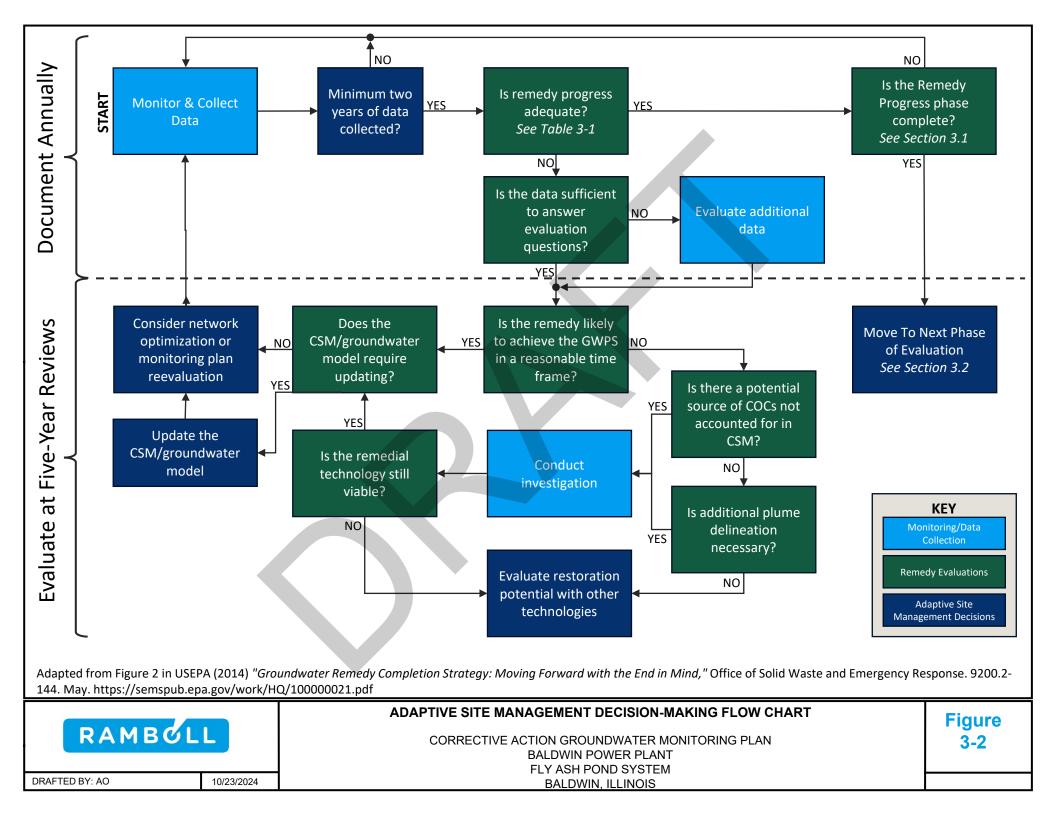
FIGURE 2-1

RAMBOLL AMERICAS ENGINEERING SOLUTIONS, INC.

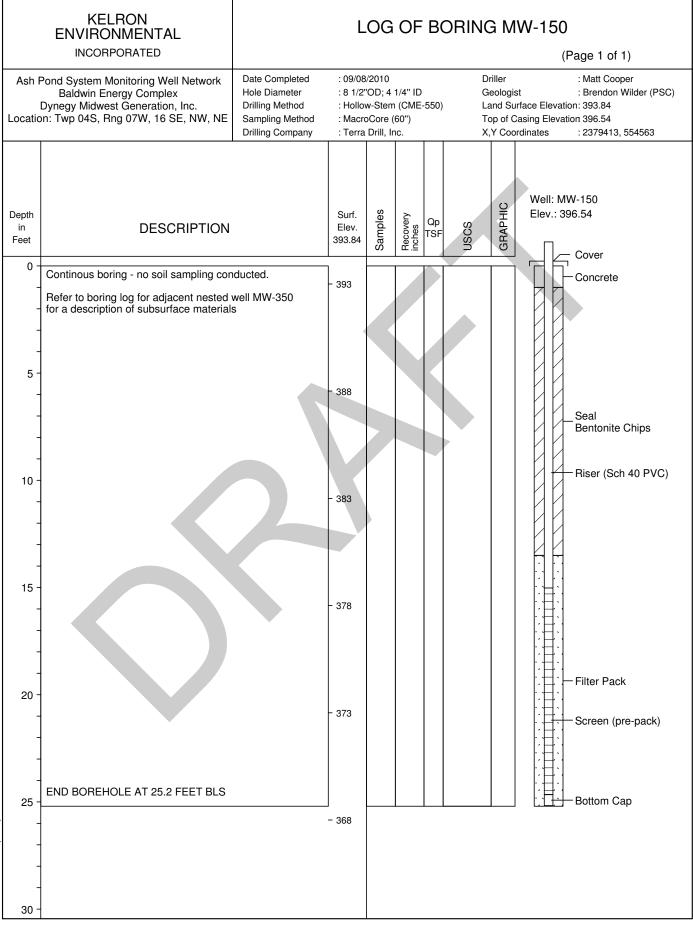


CORRECTIVE ACTION GROUNDWATER MONITORING PLAN FLY ASH POND SYSTEM BALDWIN POWER PLANT BALDWIN, ILLINOIS

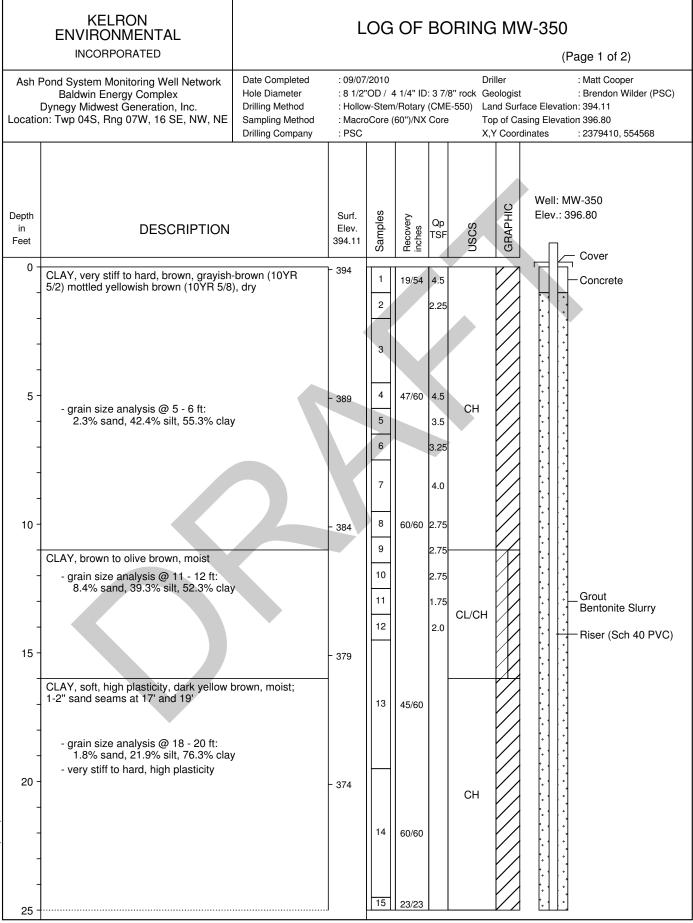






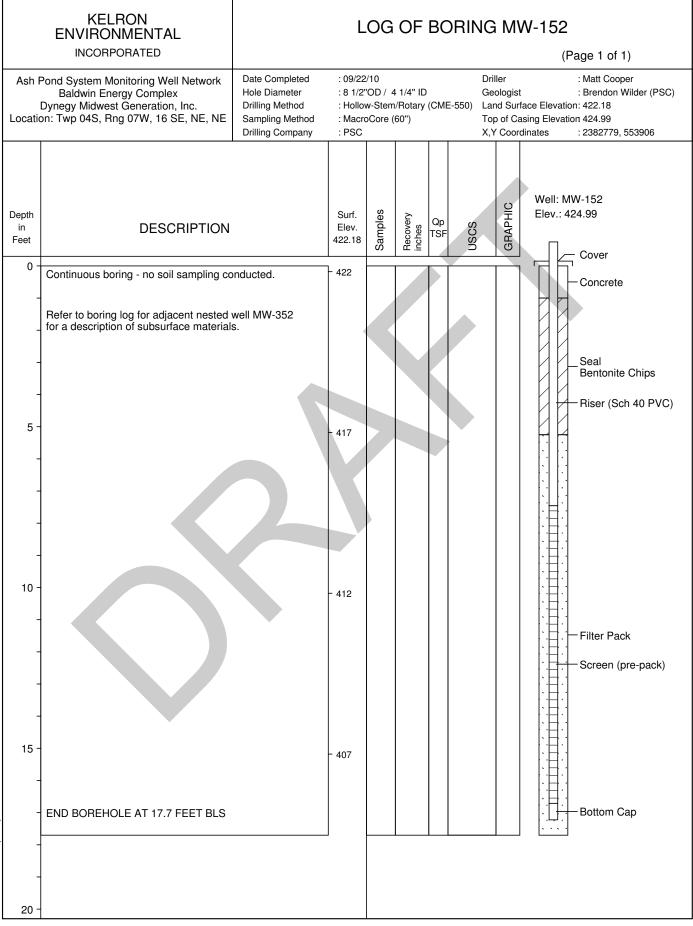


01-14-2011 c:\powerp~1\baldwin\ashmon~1\bec150~1.bor

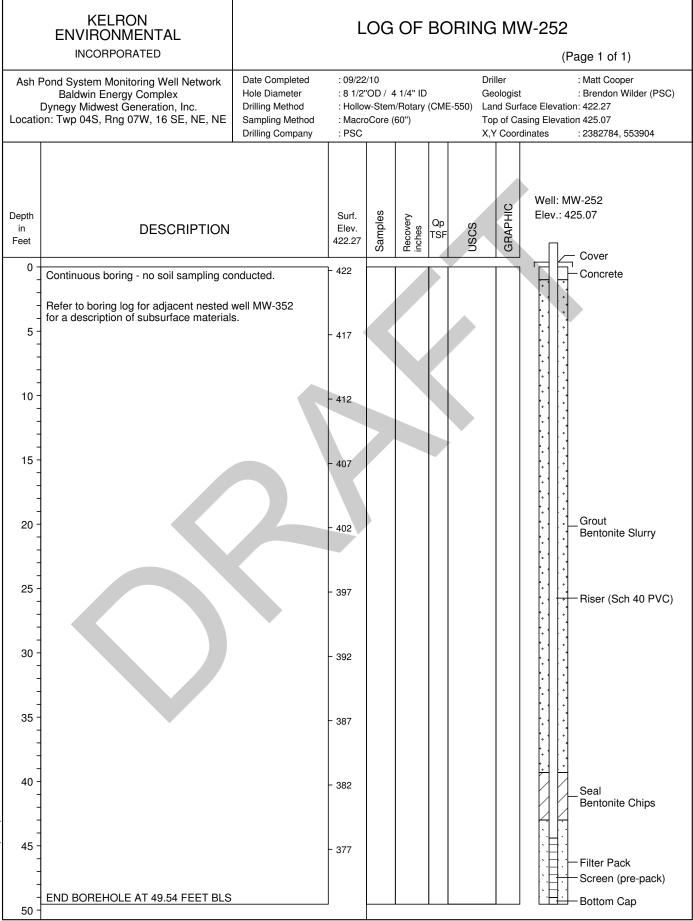


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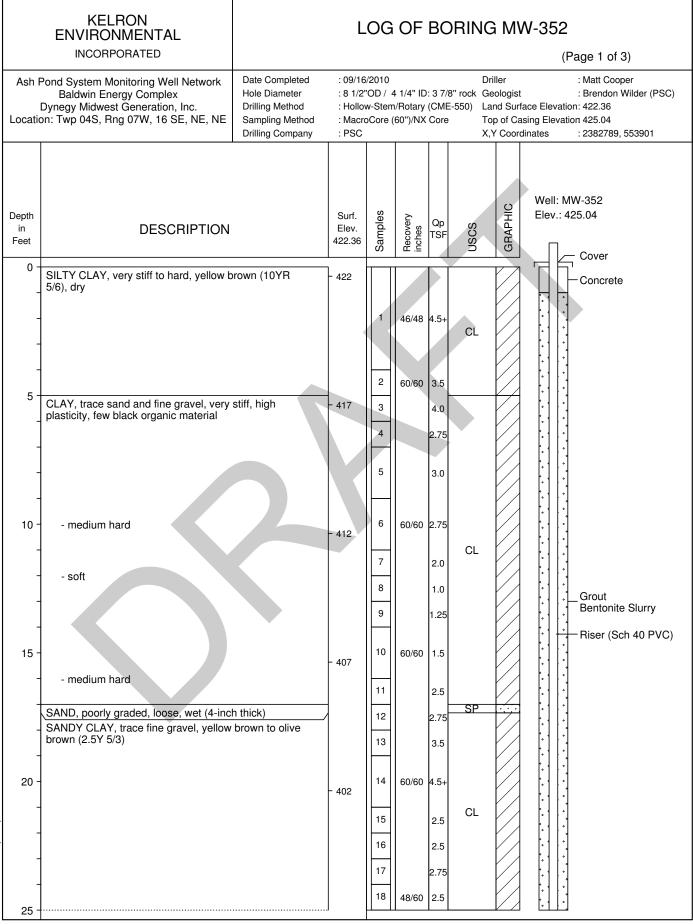
	KELRON ENVIRONMENTAL INCORPORATED		L	OG	OF	BORI	NG M\		0 (Page 2 of 2)		
	Pond System Monitoring Well Network Baldwin Energy Complex Dynegy Midwest Generation, Inc. n: Twp 04S, Rng 07W, 16 SE, NW, NE	Date Completed Hole Diameter Drilling Method Sampling Method Drilling Company	: Hollov	OD / 4		(CME-550	Top of Ca				
Depth in Feet	DESCRIPTION		Surf. Elev. 394.11	Samples	Recovery inches	Qp TSF	USCS GRAPHIC		MW-350 : 396.80		
25 - - - - - 30 - - -	- Auger refusal at 26.4 feet bgs LIMESTONE and SHALE, interbedded, very soft, light to dark gray; slightly wea LIMESTONE, banded, medium bedded medium gray; unweathered LIMESTONE and SHALE, interbedded; banded, medium bedded, hard, medium very soft to medium soft, dark gray Borehole diameter from 26.4 to 46.7 fee	solid, hard, limestone is gray; shale is	- 369	15	23/23	LS	S /SH		Grout Bentonite Slurry Seal Bentonite Chips		
- - 35 - - -	RQD for 26.4 - 36.4' = 72% (Fair) Recovery = 116/120" SHALE, banded, medium bedded, solid soft, dark gray	, soft to medium	- 359						Riser (Sch 40 PVC)		
40 -	LIMESTONE, banded, massive, solid, h hard, light to medium gray	ard to very	- 354	17	118/120		S		- Filter Pack		
45 - -	RQD for 36.4 - 46.4' = 96% (Excellent) Recovery = 118/120" END BOREHOLE AT 46.7 FEET BLS		- 349						Screen (pre-pack)		
- 50 -											



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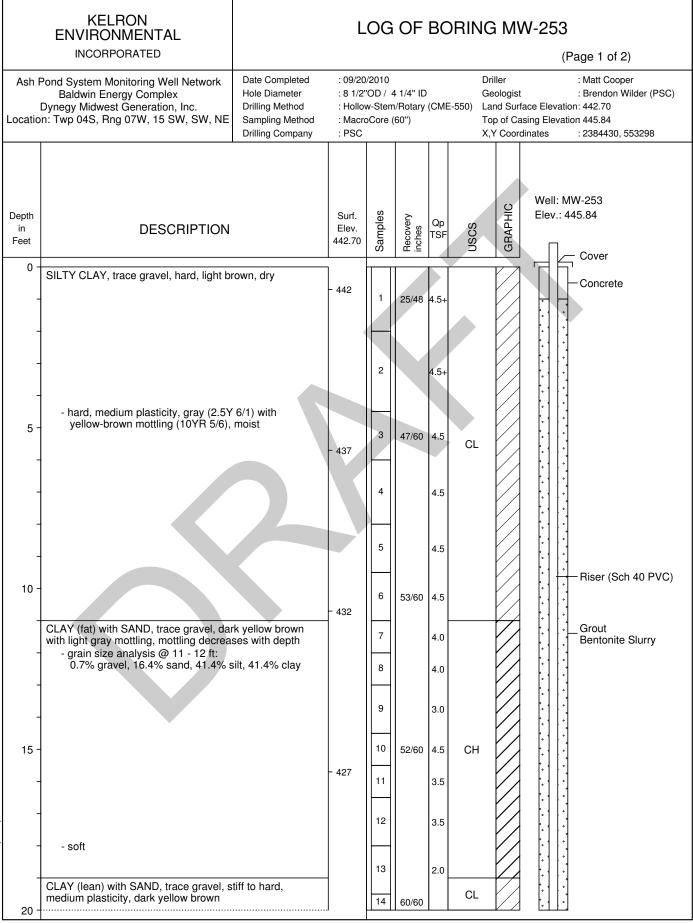
01-14-2011 c:\powerp~1\baldwin\ashmon~1\bec252~1.bor



01-14-2011 c:\powerp~1\baldwin\ashmon~1\bec352~1.bor

Ash Pord System Monitoring Well Network Dring Method Dring Corpeny Cost Cost 10 Dring Corpeny PROX PROX Dring Corpeny Dring Method Dring Corpeny Differ Dring Corpeny PROX PROX Dring Corpeny PROX PROX Dring Corpeny Differ Dring Corpeny PROX PROX Dring Corpeny PROX PROX Dring Corpeny Differ Corpet Dring Corpeny PROX PROX PROX Dring Corpeny Differ Corpet Dring Corpeny PROX PROX PROX PROX Dring Corpeny Differ Corpet Dring Corpeny PROX PROX PROX PROX PROX PROX PROX PROX		KELRON ENVIRONMENTAL INCORPORATED	LOG OF BORING MW-352 (Page 2 of 3									
Deptin Feet DESCRIPTION Stive (42236 Bit Bit (42236 Deptic Bit (42236 Deptic Bit (42336 Deptic Bit (42336 Deptic Bit (4330 Deptic Bit (4		Baldwin Energy Complex Dynegy Midwest Generation, Inc.	Hole Diameter Drilling Method Sampling Method	: 8 1/2" : Hollov : Macro	OD / 4 w-Sterr	n/Rotary	(CME-	rock Geologis 550) Land Sur Top of Ca	face Elevat asing Eleva	: Brendon Wilder (PSC) ion: 422.36 tion 425.04		
- grain size analysis @ 25.5 · 27.5 ft: 33.7% sand, 27.1% slit, 32.2% clay - <td>in</td> <td>DESCRIPTION</td> <td></td> <td>Elev.</td> <td>Samples</td> <td>Recovery inches</td> <td>Qp TSF</td> <td>USCS GRAPHIC</td> <td></td> <td></td>	in	DESCRIPTION		Elev.	Samples	Recovery inches	Qp TSF	USCS GRAPHIC				
		33.7% sand, 27.1% silt, 39.2% cla SAND with few gravel, yellow brown CLAY, some sand and fine gravel, hard high plasticity, dark yellow brown (10YR) CLAY, lean to fat - grain size analysis @ 32 - 33 ft: 13.2% sand, 43.9% silt, 42.8% cla - medium hard, high plasticity, gray b olive brown (2.5Y 5/2-5/3) - trace silt, dark yellow brown (10YR) CLAY, medium hard, low plasticity, olive	y to very hard, 4/6) brown to light 4/4)	- 392 - 387	19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35	60/60 48/60 54/60 57/60	3.0 3.0 3.5 3.0 1.5 1.5 1.75 1.75 2.0 2.5 2.0 1.75 1.75 2.5	CL/CH		Bentonite Slurry		

	KELRON ENVIRONMENTAL		L	.OG	OF BORING MW-352							
	INCORPORATED								(Page 3 of 3)			
1	Pond System Monitoring Well Network Baldwin Energy Complex Dynegy Midwest Generation, Inc. on: Twp 04S, Rng 07W, 16 SE, NE, NE	Date Completed Hole Diameter Drilling Method Sampling Method Drilling Company	: Hollov	'OD / 4 w-Sterr		Core	Land Surfa	sing Eleva	: Matt Cooper : Brendon Wilder (PSC) tion: 422.36 ation 425.04 : 2382789, 553901			
Depth in Feet	DESCRIPTION		Surf. Elev. 422.36	Samples	Recovery inches	Qp TSF	GRAPHIC		MW-352 425.04			
50 -			372				$\neg 2$		Ĵ			
-						CL			•			
	- Auger refusal at 53.7 feet bgs LIMESTONE, weathered, thinly laminate	ed, medium		37	5/5				* * *			
55 -	hard to hard, gray			38	8/27				• • •			
-			- 367			LS			Grout Bentonite Slurry			
-	SHALE, clayey, gray					SH			• • •			
- 60 -	LIMESTONE, occasional shale partings			39	19/60				•			
60 -			- 362			LS			* • •			
	- laminated, fossiliferous, medium gr	ay							Riser (Sch 40 PVC)			
-	SHALE, soft, dark gray			40	54/60				_Seal Bentonite Chips			
65 -	SHALE, SOIL, UAIK GIAY		- 357						4			
-						SH			• = • •			
	LIMESTONE, medium hard to hard, ligh	it gray		41	59/60				- - - - Filter Pack			
70 -	Borehole diameter from 53.7 to 73.8 fee	et bgs = 3 7/8"	- 352					·日				
_	RQD for 53.8 - 73.8' = 57% (Fair) Recovery = 173/240''					LS			Screen (pre-pack)			
-				42	33/34				Bottom Cap			
	END BOREHOLE AT 73.8 FEET BLS		l				──────────		<u>-</u>			
75 -												



01-14-2011 c:\powerp~1\baldwin\ashmon~1\bec253~1.bor

	KELRON ENVIRONMENTAL INCORPORATED		L	OG	OF	BORII	NG MV	
	Pond System Monitoring Well Network Baldwin Energy Complex Dynegy Midwest Generation, Inc. n: Twp 04S, Rng 07W, 15 SW, SW, NE	Date Completed Hole Diameter Drilling Method Sampling Method Drilling Company		'OD / 4 w-Sterr	-	(CME-550)		ace Elevation: 442.70 sing Elevation 445.84
Depth in Feet 20 -	DESCRIPTION - grain size analysis @ 19 - 19.5 ft: 0.7% gravel, 26.9% sand, 38.1% s	ilt, 34.3% clay	Surf. Elev. 442.70 - 422	Samples	Pecovery Inches	Qp TSF	GRAPHIC	Well: MW-253 Elev.: 445.84
- 25 -	- small fine sand seams from 25 to 2 CLAY (fat), shaley, platy/laminated, soft light yellow brown (10YR 6/4)		- 417	15	60/60	3.5		Grout Bentonite Slurry Riser (Sch 40 PVC) Seal Bentonite Chips
30 -	- stiff to very stiff, light olive brown (2 - grain size analysis @ 29 - 30 ft: 6.7% sand, 21.6% silt, 71.7% clay		- 412	17 18 19 20	60/60	3.0 4.5 3.5 3.0	T	Filter Pack
35 -	Drove split-spoon 2-inches into bec 34.7 feet bls LIMESTONE with SHALE Auger refusal at 35.0 feet END BOREHOLE AT 35.0 FEET BLS		- 407	21	2/2	LS/	SH L	· · · · · · · · · · · · · · · · · · ·
40 -								

	KELRON ENVIRONMENTAL Incorporated	LOG OF PROBEHOLE OW-257 (Page 1 of 2)										
	Phase II Hydrogeologic Investigation Baldwin Energy Complex Dynegy Midwest Generation, Inc.	Date Completed Hole Diameter Drilling Method Sampling Method Drilling Company	: 08/16 : 8 1/2' : HSA : Macro : Bulldo	' OD / 4 (CME-5 oCore (55LC) 60")	G G C	Driller : John Gates Geologist : Stuart Cravens (Kelron) Ground Elevation : 428.17 Casing (MP) Elevation : 431.02 X,Y Coordinates : 2382572, 556198					
Deptł in Feet	DESCRIPTION		Surf. Elev. 428.17	Samples	Recovery inches	Qp TSF	nscs	GRAPHIC		: OW-257 .: 431.02		
0	Continuous boring to 18.5 feet below gr Refer to boring log for adjacent well OW	ound surface. /-157.	- 425							Concrete		
ng Logs/BEC257.BOR												
11-08-2013 C:/Consulting A/Power Plants/Baldwin/Baldwin 2013 Hydrogeologic Study/Field Work Phase/Boring Logs/BEC257.BOR 0 0			- 420				CL			Seal Bentonite Grout Riser (Sch 40 PVC)		
g A\Power Plants\Baldwin\Baldwin 2013 + 51			- 415									
11-08-2013 C:\Consultin 00	- Silty CLAY, trace sand and gravel, stiff, gray (10YR 6/1) with 25-50% reddish-br moist [TILL]	high plasticity, own mottling,	- 410	1	56/60	3.0 2.75	CL					

	KELRON ENVIRONMENTAL Incorporated		LO	GΟ	F PI	ROI	BEHC	DLE C		
	nase II Hydrogeologic Investigation Baldwin Energy Complex Dynegy Midwest Generation, Inc.	Date Completed Hole Diameter Drilling Method Sampling Method Drilling Company	: HSA : Macro	' OD / 4 (CME-4 oCore			Gi Gi Ca	iller eologist round Ele asing (MF Y Coordir	vation 9) Elevatio	Page 2 of 2) : John Gates : Stuart Cravens (Kelron) : 428.17 on : 431.02 : 2382572, 556198
Depth in Feet	DESCRIPTION		Surf. Elev. 428.17	Samples	Recovery inches	Qp TSF	uscs	GRAPHIC	Well: C Elev.: 4	DW-257 431.02
20-	- >50% mottling Sandy CLAY with gravel (fine-coarse, su	ıh-angular: granite		2		2.75 2.5	CL			
-	Silty CLAY, trace sand and gravel, soft, yellowish brown (10YR5/6) with 10-25%	6), wet /	- 405	4		1.0 1.5				
25-	- very soft, brownish yellow with <10	% mottling		6	60/60	0.5 1.0				Seal Bentonite Grout
	 with trace pyrite crystals medium hardness grading to stiff 			8		2.0				
			- 400	9 10		2.0 3.25				
30-				11	60/60	1.5 3.5	CL			Riser (Sch 40 PVC)
-	 stiff, high plasticity, gray with <10% mottling, moist 	reddish-brown		13		2.75				— Seal Bentonite Chips
	- very stiff, dark gray (10YR 4/1)		- 395	14 15		2.0 3.5				
				16 17	60/60	2.0 2.0				
-	- low plasticity, very dark gray (10YR SHALE and CLAY (fat), intermittent lam dark gray, moist [note: top of weathered	nation, hard, very		18		4.0				-Filter Pack
	feet below ground surface]		- 390	19 20		3.0 >4.5	SH/CL			 Screen (pre-pack) 2"ID/3.5"OD; 4.50'open
40-	END BOREHOLE at 39.6 feet BLS			21	13/13					Bottom Cap



	/Proje	ct Nam	e		License/I	Permit/	Monitoring N	Number		Boring	y Numb	ge 1 per	01	•		
	win E	Energy	y Con				5					-366				
Boring	Drille	d By: N		f crew chief (first, last) and Firm	Date Dril	lling St	tarted	Date	e Drilli	ng Cor	npleted	1	Dril	ling Method		
	Dittm					10/0	12015			10/1	2015			1/4 HSA		
Bull	dog L	Drillin	g	Common Well Name	Einal Sta	12/3/2015 12/ Final Static Water Level Surface Elevation							2/4/2015 and rotat			
				MW-366		Feet (NAVD88) 422.54 Feet (NAVD88)								8.3 inches		
	Grid Or			stimated: 🗌) or Boring Location 🛛	· .			I		Grid Lo						
State F	Plane	555,	581.8	0 N, 2,381,171.15 Ε Ε/🛞			<u>3° 11' 31.</u>					N				
1.	1/4	of	1	/4 of Section , T N, R	Long	g <u>-89</u>				Fe	eet [S		Feet		
Facility	/ ID			County Randolph	State Illinois		Civil Town/ Baldwin	City/ or V	illage							
Sam	nle			Kandoipii	minois		Daluwiii			Soil	Prop	erties				
	(Soil/Rock Description										-		
	Length Att. & Recovered (in)	unts	Depth In Feet	And Geologic Origin For					ive (tsf)					s		
ype	th A vere	Blow Counts	l In	Each Major Unit		S	Jic	am	Compressive Strength (tsf)	Moisture Content	g	Plasticity Index	_	RQD/ Comments		
Number and Type	engl	low	eptl	Lach Major Onic		usc	Graphic Log Well	Diagram	oml	lois	Liquid	lasti ndex	200	OD III		
2 8	L R	щ		0 - 5.6' FILL, SILTY CLAY CL/ML.	_	F			0 S	20		L P	Р	0-33' Blind		
			-	-										Drilled. Se logs		
			-1					X						TPZ-166		
			-											and B-13- for soil		
			-2											description		
			_													
			-3			(FILL) CL/ML										
			_													
			-4													
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			-5													
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			-6	5.6 - 33' SILTY CLAY CL/ML.												
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						CL/ML										
						CL/ML										
						CL/ML										
			-			CL/ML										
			-			CL/ML										
			10			CL/ML										
			10			CL/ML										

Signature B Rucher	Firm Natural Resource Technology	Tel: (414) 837-3607
Brad View	234 W. Florida St., Fifth Floor, Milwaukee, WI 53204	Fax: (414) 837-3608
	Tompleter II LINOIS POPIN	CLOC Project: PALDWIN CINT CDI

Template: ILLINOIS BORING LOG - Project: BALDWIN GINT.GPJ



JGY			
	Boring Number	MW-366	

		TEC	HNOLOGY Boring Number MW-366							Pag	ge 2	of	4
Sample									Soil	Prop	erties		
Number and Type Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic 1 ac	Well	Diagram	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
		$ \begin{array}{c} 13 \\ -14 \\ -15 \\ -16 \\ -17 \\ -18 \\ -19 \\ -20 \\ -21 \\ -22 \\ -23 \\ -24 \\ -25 \\ -26 \\ -27 \\ -28 \\ -29 \\ -30 \\ -31 \\ -32 \\ \end{array} $	5.6 - 33' SILTY CLAY CL/ML. (continued)	CL/ML									



				HNOLOGY									
				Boring Number MW-366			1			 Pag		of	4
Number and Type	Length Att. & ald Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well Diagram	IIII Qui	Compressive Strength (tsf)	Liquid Limit	ţy	P 200	RQD/ Comments
1 SS	23 18	17 21 20 50	-33	5.6 - 33' SILTY CLAY CL/ML. <i>(continued)</i> 33 - 35.6' LEAN CLAY: to SHALE: CL, gray, residual soil, hard (>4.5 tsf).	CL/ML							1	
1 CORE	60 54			35.6 - 39.3' SHALE : BDX (SH), gray, highly decomposed, moderately fractured. 38.4' limestone layer (approximately 2.5").	BDX (SH)			•					Core 1, RQD=54%
2 CORIE	60 47			39.3 - 42.3' LIMESTONE : BDX (LS), cherty, intensely fractured. 42.3 - 42.9' SHALE : BDX (SH), dark gray,	BDX (LS)								Core 2, RQD=32%
3 CORIE	60 63		43 44 45 46 47 48	intensely fractured. 42.9 - 43.7' SHALEY LIMESTONE: BDX (LS/SH), intensely fractured.	BDX (SH) BDX (<u>SS</u>) BDX (SH)								Core 3, RQD=73%
4 CORE	60 49		-49 -50 -51 -52	49.8 - 54.3' SHALEY LIMESTONE : BDX (LS/SH), fossiliferous, slightly fractured.	BDX (LS/SF								Core 4, RQD=96%



			TEC	HNOLOGY Boring Number MW-366						D	4	c	1
San	nple			Boring Number 1VI VV - 300					Soil	Pag Prope		of	4
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well Diagram	Compressive Strength (tsf)	Moisture Content		Plasticity Index	P 200	RQD/ Comments
			-53	49.8 - 54.3' SHALEY LIMESTONE: BDX (LS/SH), fossiliferous, slightly fractured. <i>(continued)</i> 52.8' - 53.1 shale bed. 53.1' fossiliferous. 54.3' End of Boring.	S D BDX (LS/SH								Bedrock corehole reamed 6" in diameter to 54' for well installation.



Facilit	y/Projec	et Nan	ne		License/	Permit/	Monitori	ing Nu	ımber		Boring	Pag Numb	, ,	of	0	
			y Con										-384			
-		•	Name o	f crew chief (first, last) and Firm	Date Dri	lling St	arted		Dat	e Drilli	ing Con	npleted			ing Metho	
	d Dut					10/7	/2015			1	12/16/	2015			l/4 HSA	
Dui	ldog E	<u>лпп</u>	Ig	Common Well Name	Final Sta				Surface	e Eleva		2013	Bo		d rotary Diameter	
				MW-384			VD88				eet (N.	AVD8			3 inches	
	Grid Or			stimated:) or Boring Location	1			30.4			Grid Lo					
State 1				1 N, 2,384,518.72 E E/⊛		t <u>38</u>							N			
Facilit	1/4 v ID	of	1	/4 of Section , T N, R County	Long		Civil To	<u>38.5</u>		/illage	Fe	et 🗋] S]	Feet	V
i acini	y ID				Illinois		Baldw		ty/ OI	rinage						
San	nple										Soil	Prope	erties			
	<u> </u>		t	Soil/Rock Description												
	dt. 8 sd (i	unts	Fee	And Geologic Origin For						sive (tsf)					ts	
lber Type	gth A overe	v Co	h In	Each Major Unit		SCS	hic	ram		pres	sture	t Ed	icity x	0	o/ men	
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet			U S	Graphic Log	Well Diagram		Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments	
1 SS //	24	2 3 4	-	0 - 2.5' FILL, ASH (Coal): very soft to mode	erately			98								
ss	8	4 6	E	stiff (0-0.75 tsf).			k	88								
ΙŇ			-1			(FILL)			1							
			E													
2	24	2	-2													
2 SS	19	2 4 3 6	E	2.5 - 4' FILL, SILTY CLAY CL/ML, strong b	rown											
X			-3	(7.5YR 4/6), trace gravel, very soft to very st (0-3.5 tsf).	tiff	(FILL) CL/ML										
M			F	(0-3.3 (5)).		CL/ML										
3 H	24	1	-4	4 - 18' FILL, ASH (Coal): yellowish red (5YI	R 4/6)											
3 SS	10	1 2 3 4	-	to reddish black (10R 2.5/1), sand-sized ash	and											
X			-5	cinders, very soft to stiff (0-1.5 tsf).												
M			E													
AH	24	2	-6													
4 SS	24	2 2 2 2	E													
I.V.		2	-7													
IA			E													
_ []			-8			(FILL)										
5 SS	24	1 2 1	E T													
Į		1	– 9													
IA			Ę													
			- 10													
6 SS	24	1 2 1 1	10													
		1	 													
۱۸			-11													
$ \rangle$			ŧ.													
			-12													
hereb	y certif	y that	the info	rmation on this form is true and correct to the bes	st of my ki	nowledg	ge.									

Signature	Firm Natural Resource Technology	Tel: (414) 837-3607
	234 W. Florida St., Fifth Floor, Milwaukee, WI 53204	Fax: (414) 837-3608
	Templeter II I INOIS PODIN	CLOC Droject: PALDWIN CINT CDI

Template: ILLINOIS BORING LOG - Project: BALDWIN GINT.GPJ



			TEC	HNOLOGY Boring Number MW-384							Pag	ge 2	of	6
Sar	nple									Soil	Prop	erties		_
S > Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well Diagram)	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
7 SS	24	1 5 10 10	-13	4 - 18' FILL, ASH (Coal) : yellowish red (5YR 4/6) to reddish black (10R 2.5/1), sand-sized ash and cinders, very soft to stiff (0-1.5 tsf). <i>(continued)</i>						20		Η	H	
8 SS	24 14	5 10 11 11	-14	14' wet.	(FILL)									
9 SS	24 14	5 8 14 15						•						
10 SS	24 16	2 2 3 4	- 18	18 - 22' SILTY CLAY CL/ML, gray (5Y 6/1), organic odor, stiff to very stiff (1.25-3.75 tsf), wet.										
11 SS	24 18	2 2 6 4	-20		CL/ML									
12 SS	24 16	4 4 5 4	-22	22 - 24' SILT : ML, very dark gray (10YR 3/1), dark yellowish brown (10YR 3/6) mottling, hard (4.25-4.5 tsf).										
13 SS	24 22	1 2 5 7	-24	24 - 42.4' SILTY CLAY CL/ML, gray (10YR 5/1) with yellowish brown (10YR 5/8), oxidation staining, very soft to hard (<0.25-4.5+ tsf).										Permanent 6" PVC casing set
14 SS	24 21	3 4 5 7	-26 -27	26' yellowish brown (10YR 5/4), trace yellowish brown (10YR 5/8) and very dark gray (10YR 3/1) mottling, 15-30% silt, 5-15% fine sand, trace fine gravel, stiff to very stiff (1.25-2.5 tsf), low to medium plasticity, moist.										at 25' bgs.
15 SS	24 21	3 4 5 6	-28	28' color grades to gray (10YR 5/1), 30-50% silt, soft to stiff (0.5-1.25 tsf).	CL/ML									
16 SS	24 17.5	1 5 5 7		30' yellowish brown (10YR 5/8) mottling (15-30%), trace very dark gray (10YR 3/1) mottling, no gravel, very soft to very stiff (<0.25-2.5 tsf), medium plasticity.										



				Boring Number MW-384							Pa	ge 3	of	6
San	nple									Soil	Prop	erties		
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Loo	Well	Diagram	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
17 SS	24 20.5	4 4 6		24 - 42.4' SILTY CLAY CL/ML, gray (10YR 5/1) with yellowish brown (10YR 5/8), oxidation staining, very soft to hard (<0.25-4.5+ tsf). <i>(continued)</i> 32' trace yellowish brown (10YR 5/8) and very dark gray (10YR 3/1) mottling, 15-30% silt, stiff to very stiff (1.75-3.5 tsf).										
18 SS	24 22	3 4 5 7	-34	34' yellowish brown (10YR 5/8) mottling (15-30%), trace very dark gray (10YR 3/1) mottling, stiff to very stiff (1.5-2.5), dry to moist.										
19 SS	24 21	4 3 3 4	-36	35.3' yellowish brown (10YR 5/8), trace gray (10YR 5/1) and very dark gray (10YR 3/1) mottling. 36' gray (10YR 5/1) mottling (15-30%), silt content increasing with depth, moderately stiff to stiff (0.75-1.25 tsf), low plasticity, moist.	CL/MI			•						
20 SS	24 24	2 4 7 14	-38	38' grayish brown (10YR 5/2), trace gray (10YR 5/1), trace strong brown (7.5YR 4/6) mottling, 30-50% silt, soft to very stiff (0.5-3.75 tsf). 38.7' - 40' very dark gray (10YR 3/1) mottling (5-15%), 5-15% fine gravel.										
21 SS	24 25	3 11 21 44	-40 41	40' sand (5-15%), trace gravel, very stiff to hard (3.5-4.5+ tsf). 40.3' wet. 40.8' very stiff to hard (3.5-4.5+ tsf), moist.										
22 SS	24 20	13 11 15 17	-42 -43	41.8' fine sand seam (1/4" thick). 42' - 42.4' fine gravel, 30-50% clay, trace sand, wet. 42.4 - 44.3' CLAYEY SILT ML/CL, gray (10YR 5/1) to grayish brown (10YR 5/2), 30-50% clay, 5-15% fine sand, trace subrounded gravel, very stiff	ML/CI									
23 SS	24 17	6 8 10 14	-44 -45	to hard (3.5-4.5+), nonplastic to low plasticity, moist. 43.5' - 44.3' very dark grayish brown (10YR 3/2), brownish yellow trace (10YR 6/6) mottling, trace // coal. // 44.3 - 56' LEAN CLAY: CL, brownish yellow trace										
24 SS	24 16	5 10 11 15		(10YR 6/6), trace light brownish gray (10YR 6/2) mottling, 15-30% silt, 5-15% gravel, trace gravel-sized oxidation-stained nodules, very stiff (2.5-3.0 tsf), low to medium plasticity, moist to dry. 46' decreasing silt content, trace gravel, clay becoming laminated with depth, very stiff (2.25-3.0 tsf).										
25 SS	24 13.5	6 8 12 22	-48 -49	48' silt (5-15%), trace shale gravel, very stiff (3.0 tsf), medium plasticity, dry.	CL									
26 SS	24 16	8 9 15 19	-50 -51 -52	49.2' gravel (2" diameter). 50' very dark grayish brown (10YR 3/2) to dark grayish brown (10YR 4/2), trace silt, very stiff (3.5 tsf), medium to high plasticity, highly weathered shale (residual soil).										



			TEC	HNOLOGY Boring Number MW-384							Pa	ge 4	of	6
San	nple									Soil	Prop	erties		
2 Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well Diagram	þ	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
27 SS	24 22	13 14 9 14	53	44.3 - 56' LEAN CLAY : CL, brownish yellow trace (10YR 6/6), trace light brownish gray (10YR 6/2) mottling, 15-30% silt, 5-15% gravel, trace gravel-sized oxidation-stained nodules, very stiff (2.5-3.0 tsf), low to medium plasticity, moist to dry. <i>(continued)</i>										
28 SS	24 24	12 12 14 22	-54	52' - 54' clay is fractured, light brownish gray (10YR 6/2) to light yellowish brown (10YR 6/4) in fractures. 54' trace very dark brown (10YR 2/2) laminations, hard (>4.5 tsf).	CL									
29 SS 1 CORE	23 20 24 40	11 14 20 50/5"		56 - 58.2' SHALE: BDX (SH), very dark gray (10YR 3/1), highly weathered, fissile, totally healed fractures, very weak, highly decomposed [light brownish gray (10YR 6/2) in fractures], very intensely fractured (closed to narrow apertures). 57' light yellowish brown (10YR 6/4) to very dark gray (10YR 3/1) layers, thinly bedded, highly	BDX (SH)			Þ						3" steel casing set at 57.7 ft bgs. Core 1, RQD=36%
2 CORE	60 64			decomposed to residual soil. 58.2 - 60.8' LIMESTONE: BDX (LS), light greenish gray (GLEY 1 7/10Y), microcrystalline, trace fossils, moderately strong to strong, medium bedded, slightly to moderately decomposed, moderately fractured.	BDX (LS)									Core 2, RQD=73%
3 CORIE	60 73		61 62 63 64 64	64 - 82.6' SHALE: BDX (SH), greenish gray (GLEY 1 5/10Y), very weak, thinly bedded, highly to moderately decomposed, slightly to moderately disintegrated, intensely fractured (very narrow to	BDX (LS/SH									Core 3, RQD= 58%
4 CORIE	60 63		-66 -67 -68 -69 -70 -71	 67.9' - 68.8' shale clasts within decomposed shale matrix. 68.8' - 69.2' light yellowish brown (10YR 6/4), trace dark yellowish brown (10YR 3/6) layers. 69.2' - 74' intensely fractured (extremely narrow to narrow aperture). 	BDX (SH)									Core 4, RQD=46%
			-72											



			TEC	HNOLOGY						_	~		7
San	nple			Boring Number MW-384					Soil		ge 5 erties	of	0
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well Diagram	Compressive Strength (tsf)	Moisture Content		ty	P 200	RQD/ Comments
5 CORE	60 20	I	73 74 75 76	 64 - 82.6' SHALE: BDX (SH), greenish gray (GLEY 1 5/10Y), very weak, thinly bedded, highly to moderately decomposed, slightly to moderately disintegrated, intensely fractured (very narrow to moderately narrow apertures). <i>(continued)</i> 74' - 79' intensely to very intensely fractured. 	1						I	H	Core 5, RQD=0%
6 CORE	60 64		-77 -78 -79 -80 81	79' - 82.6' intensely fractured.	BDX (SH)								Bedrock corehole reamed 6" in diameter to 77' for well installation. Core 6, RQD=64%
7 CORIE	60 37	-		 82.6 - 83.9' SHALEY LIMESTONE: BDX (LS/SH), light greenish gray (GLEY 1 7/10Y), fossiliferous, intensely fractured (extremely narrow to narrow apertures), slightly decomposed. 83.9 - 85.6' SHALE: BDX (SH), greenish gray (GLEY 1 5/10Y), very weak, medium bedded, highly to moderately decomposed, slightly to moderately disintegrated, intensely fractured (extremely narrow to narrow apertures). 85.6 - 88.7' SHALEY LIMESTONE: BDX (LS/SH), light greenish gray (GLEY 1 7/10Y), shaley, fossiliferous, intensely fractured (extremely narrow 	BDX (LS/SH BDX (SH)								Core 7, RQD=15%
8 CORIE	60 50		87 88 89 90 91 92	to narrow apertures), slightly decomposed. 86.4' - 87' SHALE layer, greenish gray (GLEY 1 5/10Y), very weak, medium bedded. 88.7 - 94.1' SHALE: BDX (SH), greenish gray (GLEY 1 5/10Y), very weak, medium bedded, highly to moderately decomposed, slightly to moderately disintegrated, intensely fractured (extremely narrow to narrow apertures).	BDX (LS/SH BDX (SH)								Core 8, RQD=49%



		TEC	HNOLOGY								
Sample			Boring Number MW-384	1				Soil	age 6 perties	of	6
Number and Type Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	JSCS	Graphic Log	Well Diagram	Compressive Strength (tsf)	Moisture	Plasticity Index	P 200	RQD/ Comments
		-93	88.7 - 94.1' SHALE: BDX (SH), greenish gray (GLEY 1 5/10Y), very weak, medium bedded, highly to moderately decomposed, slightly to moderately disintegrated, intensely fractured (extremely narrow to narrow apertures). (continued) 92.5' - 93.2' light greenish gray (GLEY 1 7/10Y), shaley, fossiliferous, intensely fractured, slightly decomposed. 94.1' End of Boring.	D BDX (SH)							



	/Projec				License/I	Permit/	Monitoring	Numb	ber		Pag Numb	er	of 2	
			y Com								PZ-1			
•		-	Name o	f crew chief (first, last) and Firm	Date Dri	lling St	arted		Date Drill	ing Cor	npleted			ng Method
	d Dutt					0/1/	2015			8/4/2	015			low stem
Duii	dog D	111111	ıg	Common Well Name	Final Sta			Sur	face Eleva		015	Bo	aug rehole	Diameter
				PZ-174			AVD88)		398.97 F		AVD8			3 inches
local (Grid Or	igin	(es	stimated:) or Boring Location			,		Local	Grid Lo		•)		
State I	Plane	554	,666.2	3 N, 2,379,774.23 Е Е/🛞	La	t <u>38</u>]N		
	1/4	of	1	/4 of Section , T N, R	Long					Fe	et 🗌]S	I	Feet
Facility	/ ID			2	State		Civil Town	~	or Village					
0	1			Randolph	Illinois		Baldwin			0.11	D			
Sam										Soil	Prope	erties		
	(ii) &	ıts	eet	Soil/Rock Description					e ce					
be r	Att	Jour	In Fe	And Geologic Origin For		s	0	я	essi ^r h (ts	t e		ty		ents
Number and Type	ngth	Blow Counts	Depth In Feet	Each Major Unit		U	Graphic Log Well	Diagram	Compressive Strength (tsf)	Moisture Content	Liquid	Plasticity Index	200	RQD/ Comments
and	Length Att. & Recovered (in)	Blc	De			U.S	Grap Log Well	Dia	Str Str	C Mo	Liquic Limit	Plastic Index	P 2	Co. Co
1 SS \/	24 5	2 3 5 3	È _	0 - 2' TOPSOIL: ML, brown (10YR 4/3), trac grass and roots, cohesive, nonplastic, dry.	e –		[↓ *]							
Ĩ	Ŭ	3	F.					X						
M						ML	\downarrow \downarrow							
\mathbb{N}			F											
2 55	24	2	-2	2 - 4' No Recovery.										
s	0	2 2 2 4	F											
X			-3											
			F											
2 H	24	2	-4	4 - 24.7' LEAN CLAY: CL, dark grayish brow										
3 SS	6	2 2 4 5	E	(10YR 4/2), dark vellowish brown (10YR 4/4)										
- IVI		5	-5	mottling, sílt (10-20%), cohesive, medium plá moist.	sticity,									
M			F											
			E-6											
4 SS	24 6	4 4 5 7	Ę											
,	0	5	F_											
M			E'											
			E											
5 SS	24	3	-8	8' - 9.9' increased yellowish brown (10YR 4/	4)	CL								
s	23	3 4 5 5	F	mottling, increase in silt content with depth (50%).									
X			-9											
Α			E											
. Ц			-10											
ŝ	24 20	2 4 8 6	F	10' - 11.7' decrease in silt content with depth (10-20%).	1									
- [V]		ē	E	10.6' - 11.2' dark yellowish brown (10YR 4/4										
			11	very dark brown (10YR 2/2) mottling (50%), o moist.	ary to									
M			1			1			1	1	1	ı		
\wedge			-12											

Signature Park M Haff	Firm Natural Resource Technology 234 W. Florida St., Fifth Floor, Milwaukee, WI 53204	Tel: (414) 837-3607 Fax: (414) 837-3608
	Template: ILLINOIS BORIN	G LOG - Project: BALDWIN GINT.GPJ



			TEC	HNOLOGY Boring Number PZ-174						Pag	ge 2	of	2
Sar	nple								Soil	Prop			
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	SCS	Graphic Log	Well Diagram	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
Z B 7 SS	<u>24</u> 21	8 2 3 5 7	13	4 - 24.7' LEAN CLAY: CL, dark grayish brown (10YR 4/2), dark yellowish brown (10YR 4/4) mottling, silt (10-20%), cohesive, medium plasticity, moist. <i>(continued)</i> 12' - 13.8' trace coarse sand, dry.	Ω	Pro	D	<u>x c</u>	Ŭ		PI	P	~ ~ ~
8 SS	24 21	2 4 5 8	-14	14' - 15.8' increased sand content, trace gravel, dry.									
9 SS	24 24	2 4 5 7		16' - 18' yellowish brown (10YR 5/4), moist.									
10 SS	24 24	3 7 9 12	- 18	18' - 20' coarse sand and gravel (5-15%), moist.	CL								
11 SS	24 24	3 7 9 15	-20										
12 SS	24 24	4 7 8 10	-22 -23										
13 SS	88	11 50 for 2*	24	24' - 24.7' decreased moisture content with depth. 24.7' End of Boring.									Hollow Stem Auger Refusal at 24.7 ft bgs on Shale Bedrock.



			TEC	HNOLOGY							Pag	ge 1	of	2
	y/Projec				License/	Permit/	'Monitoring N	lumber		Boring				
	lwin E			plex f crew chief (first, last) and Firm	Date Dri	Iling St	tarted	Date	Drilli	ing Cor	PZ-1		Drill	ing Method
~	d Dutt	-		rerew enter (first, fast) and Firm	Date Di	ining 5	laiteu	Date	DIIII		ipieteu			llow stem
	ldog D		g			8/6/	2015			8/6/2	015			ger
			-	Common Well Name			ter Level	Surface						Diameter
Local	Grid Or	ioin		PZ-176 stimated: □) or Boring Location ⊠	Fe	et (NA	AVD88)			eet (N Grid Lo		88)	8	.3 inches
State 1				6 N, 2,381,381.02 E E/(W)	La	ut <u>38</u>	<u>8° 11' 18</u>	<u>8.834 "</u>]N		E
	1/4			/4 of Section , T N, R	Lon	g <u>-89</u>	<u>9° 52' 17.</u>	8428"		Fe	-]S]	Feet W
Facility	y ID				State	-	Civil Town/C	ity/ or V	illage					
	1		1	Randolph	Illinois		Baldwin			<u> </u>	<u> </u>			
San	-							1		Soil	Prope	erties		
	Length Att. & Recovered (in)	ats	eet	Soil/Rock Description					sf)					
er Pe	ı Att ered	Cour	In F	And Geologic Origin For		s	<u>्</u> र ह		essi th (t	t ie		ity		ents
Number and Type	ngth	Blow Counts	Depth In Feet	Each Major Unit		SC	Graphic Log Well Diagram	n P1 9	Compressive Strength (tsf)	Moisture Content	Liquid	Plasticity Index	200	RQD/ Comments
	P Le		<u> </u>			ÛS	Grap Grap Log Well		S S	Σŭ	E E	Pl: In	Р	<u> </u>
1 SS	24 15	3 3 4 4		0 - 0.5' TOPSOIL: ML, dark grayish brown (⁻ , 4/2), clay (5-15%), trace grass and roots, coh	iorra iesive, _/	<u>ML</u>)						
Į		4	-1	nonplastic, stiff (1.5 tsf), dry. 0.5 - 2.4' SILT: ML, dark gravish brown (10Y										
I/			F	brownish yellow (10YR 6/6) and dark brown (10YR	ML								
			-2	3/3) mottling, clay (30-50%), trace roots, cohe low plasticity, very stiff (3.0 tsf), dry.	esive,	IVIL								
2 SS	24 16	3 3 5 5	- 1											
		5	F,	2.4 - 6.3' LEAN CLAY: CL, dark yellowish br (10YR 4/4), dark gray (10YR 4/1) mottling, sil										
IV.			-3	(5-15%), trace roots, cohesive, medium plasti moist.	icity,									
			F.	moist.										
3	24	2 3 4 4	<u>–</u> 4	4' increase in silt content (40-60%), dry to mo	oist.									
ss	9	4 4	F			CL								
I Å			-5											
			E											
4	24	3	-6			L								
ss	21	3 3 3 4	Ē	6.3 - 12' SILT: ML, dark gray (10YR 4/1), col nonplastic, moist.	nesive,									
X			-7	honpidotic, molot										
\wedge			2											
5	24	1	-8	8' sand (0-40%), sand content increasing wit	h depth,									
5 SS	12	1 1 2	F	moist to wet.	• •									
X			<u>-</u> 9											
			F			ML								
e H	24	1	-10	10' increase in sand content (40-60%).										
6 SS	13	1 1 2	E											
I Y		2	-11											
\Box			-12			L								
I hereb	by certif	y that	the info	brmation on this form is true and correct to the be	st of my k	nowled	lge.	1						
Signat	ure			Firm Natur			Technology				Tel	(414)	837-36	07
		1 pm	LM				th Floor, Milw				Fax:	(414)	837-36	08
	V						Temp	late: ILLI	NOIS E	BORING	LOG -	Project:	BALD	WIN GINT.GPJ



Samt and Type SS S	PR Length Att. & G Recovered (in)	Blow Counts	Feet	Soil/Rock Description						Soil	Prop	erties		
Number and Type	Recovered (in)	v Counts	Feet	Soil/Rock Description										-
7	24	Blov	Depth In Feet	And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well Diagram	0	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
55	20	1 2 3 5	-13	12 - 12.3' WELL-GRADED SAND: SW, very dark grayish brown (10YR 3/2), fine gravel (>15%), moist. / 12.3 - 16' LEAN CLAY: CL, gray (10YR 5/1), brownish yellow (5-15% 10YR 6/6) and trace very dark brown (10YR 2/2) mottling, silt (5-15%), trace sand seams, cohesive, medium plasticity, stiff to	1 <u>.sw</u>									
8 SS	24	2 3 5	-14	very stiff (1.5-3.0 tsf). 14' increase in thickness of sand seams (1"-2" thick, moist, wet).	CL									
9 SS	24 17	2 4 7 10	-17	16 - 28.6' LEAN CLAY: CL, dark gray (10YR 4/1), light yellowish brown (10YR 6/4) mottling, cohesive, low plasticity, very stiff to hard (3.5->4.5 tsf) dry.										
10 SS	24 18	4 6 8 12	-19	18' increased mottling, mostly brown (10YR 5/3), brownish yellow (10YR 6/6), dark gray (10YR 4/1), and olive gray (5Y 5/2) mottling.										
11 SS	24 17	5 16 22 25	-21	20' olive gray (5Y 5/2), brownish yellow (10YR 6/6) mottling. 20.3' dark gray (2.5Y 4/1), brownish yellow (10YR 6/6) mottling, clay becoming blocky and laminated.										
12 SS	11 7	7 50 for 5"	-23	22' pale olive (5Y 6/3), dark gray (10YR 4/1) mottling, laminated.	CL									At 23.6' rock
13 SS	24 24	13 21 31 43	-25	24' brownish yellow (10YR 6/6) mottling.										fragment on bottom of split spoon. Refusal of split spoon.
14 SS	24 24	14 12 17 19	26											
15 SS 16 SS	8 8 1 0	9 50 for 2" 50 for 1"	-28	28' hard (4.5 tsf). 28.6' End of Boring.										



Facilit	y/Projec	et Nam	ne		License/	/Permit/N	Ionito	ring N	umbe	er	Borin	Pa g Numb		of	3	
Bal	dwin P	ower	Plant					0				MW	/-253			
		•	Name o	f crew chief (first, last) and Firm	Date Dr	illing Sta	rted		I	Date Dril	ling Co	mpletec	1	Drill	ing Met	hod
Eth	an Ora scade I	unge Drillir	ng LP			5/1/2	2024				5/1/2	2024		Sc	nic	
			0	Common Well Name		atic Wate	er Leve		Surfa	ace Elev	ation		Borehole Diameter			
Local	Grid Or	inin		MW-253R stimated:) or Boring Location	Fe	eet (NA	VD88	8)			(NAV Grid La			6	.0 incl	ies
	Plane	ngin	[] (e	stimated: \Box) or Boring Location \boxtimes N, E N/C/S	La	at		<u>'</u>		- Local	Grid Lo		□N			Β
	1/4	of	1	1/4 of Section , T N, R	Lon			<u>'</u>		"					Feet	
Facilit	y ID			-	State				ity/ o	r Village	;					
	1			Randolph	IL		Baldy	win			0.1	1 D				
Sar	mple											l Prop			-	
	tt. & d (in	unts	Feet	Soil/Rock Description And Geologic Origin For						sive teft	Te					S
ber Type	th A vere	Col	h In	Each Major Unit		S ()	hic	ram		press	ture	P.	icity			ment
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet			USCS	Graphic Log	Well Diagram	Ò	Compressive Strength (164)	Moisture	Liquid	Plasticity Index	P 200	RQD/	Com
1	120			0 - 10.2' SILTY CLAY: CL/ML, brown (10YF	R 5/3),		ŽĪ									<u> </u>
CS	120		Ē	gravel (0-10%), hard, dry.												
			1						X							
			Ē													
			E^{-2}	2.2' strong brown (7.5YR 4/6) mottling (20-3	0%)											
			Ę	light gray (2.5Y 7/1) mottling (20-30%), very	dark											
			-3	gray (10YR 3/1) móttling (0-10%).			\geq									
			E													
			-4													
			È,													
			5			CL/ML										
			-													
			E ⁻⁶													
			F _													
			Ē													
			È													
			-8													
			-													
			-9													
			-													
2 CS	120 120		-10	10.2 - 15.4' SILTY CLAY WITH SAND: (CL	/ML)S.		<u>/</u>									
63	120		- - 	brown (10YR 5/3), strong brown (7.5YR 4/6) (20-30%), light gray (2.5Y 7/1) mottling (20-3	mottling											
				very dark gray (10YR 3/1) mottling (0-10%),	gravel	(CL/ML)				3.5						
			-12	(0-10%), medium to high plasticity, moist.												
	hv certif	fy that		prmation on this form is true and correct to the bo	est of my 1	knowled	<u>те</u>		1			1				
Signat	-	iy mat		Firm Ram		kilowied	<u>5</u> 0.					T-1	. (114)	027 24	07	
0	5	-	- 6	han Ram	10011							rel	: (414)	03/-30	107	

gnature	6 62	Firm Ramboll	Tel: (414) 837-3607
	~~~ <i>fc</i> ~	234 W. Florida St., Fifth Floor, Milwaukee, WI 53204	Fax: (414) 837-3608
		Template: RAMBOLL MINNESOTA ROPING LOG	Project: NE BALDWIN 2024 CPL

Template: RAMBOLL MINNESOTA BORING LOG - Project: NE_BALDWIN_2024.GPJ



~			· · · · ·	Boring Number MW-253R						~ .		Page 2	of	3
Sampl										Soi	l Pro	perties		-
Number and Type Length Att. &		Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well	Diagram	Compressive Strength (tsf)	Moisture Content	Liquid	Limit Plasticity Index	P 200	RQD/ Comments
3 1	120		$ \begin{array}{c}     13 \\     -14 \\     -15 \\     -16 \\     -17 \\     -18 \\     -19 \\     -20 \\     -21 \\     -22 \\     -23 \\     -24 \\     -25 \\     -26 \\     -27 \\     -28 \\     -28 \\   \end{array} $	15.4 - 18.2' <b>LEAN CLAY WITH SAND:</b> (CL)s, yellowish brown (10YR 5/4), gravel (0-10%), medium plasticity, moist. 18.2 - 27.2' <b>SILTY CLAY WITH SAND:</b> (CL/ML)S, yellowish brown (10YR 5/4), strong brown (7.5YR 4/6) mottling (10-20%), light gray (2.5Y 7/1) mottling (10-20%), very dark gray (10YR 3/1) mottling (0-10%), sand (10-20%), gravel (0-10%), moist. 20' gravel (10-20%). 22' - 25' intermittent fine sand seams.					2.5 1.5 1 3 3.5 3.5 3.5 3.5 4.5 4.5					
4 ( CS (	60 60		-29 30 31 32	light olive brown (2.5Y 5/4), weathered shale, laminated.	BDX (SH)									

# RAMBOLL

				Boring Number MW-253R						Pa	.ge 3	of	3
San	nple								Soil	Prop	erties		
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	S C S	Graphic Log	Well Diagram	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
			-33	28.3 - 35' Weathered SHALE Bedrock: BDX (SH), light olive brown (2.5Y 5/4), weathered shale, laminated. (continued) 35' End of Boring.	D BDX (SH)								



<b>F</b> 114	/ <b>D</b> :					<b>T</b> • • • •	<b>D</b>	<u></u>		T 1			Pag		of	3
Facility Bald	//Projec lwin P					License/	Permit/	vionito	oring N	umber		Boring		er -350	R	
				f crew chief (first, last) and Firm		Date Dr	illing St	arted		D	ate Drill					ing Method
Etha	in Ora cade E	inge Frillin	σID				5/3/	2024				5/3/2	024		S	onic
Case		<u>лшш</u>	g Lr	Common	Well Name	Final Sta				Surfa	ce Eleva		024	Bo		Diameter
					-350R	Fe	et (NA	AVD8	(88			(NAV			6	.0 inches
Local C State 1		rigin		stimated: 🗌 ) or Boring Locatio N, E N	n ⊠ /C/S	La	at	°	'	"	Local	Grid Lo		٦		
	1/4	of	1	,	, R	Lon	g	°	'	"		Fe		]N ]S		□ E Feet □ W
Facility	/ ID			County		State				City/ or	Village					
San	mla			Randolph		IL		Bald	win			Soil	Prope	ortion		
Sall				Soil/Rock Descrip	tion							5011	Flope			-
0	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	And Geologic Orig							Compressive Strength (tsf)					Its
Number and Type	gth A overe	v Co	th In	Each Major Ur			CS	Graphic Log	Well		Compressive Strength (tsf)	sture	E. E.	Plasticity Index	0	RQD/ Comments
Nun and	Len Rec	Blov	Dep				USC:	Grap Log	Well	-Tra	Con Stre	Moisture Content	Liquid Limit	Plastic Index	P 200	RQI Con
1 CS	120 120		_	0 - 14.4' <b>SILTY CLAY:</b> CL/ML, g (10YR 5/2), yellowish brown (10)	'R 5/8) mottl	ling				Š						
			-1	(30-40%), organics material and medium to high toughness, low to	roots (0-10%	b),					1.5					
				moist.		·····,					1.5					
			-2							•						
			-3								2					
			-4													
			_													
			-5								2.5					
			-													
			-6				CL/ML									
			-7													
			E'								3					
			-8													
			Ē													
			-9								4.5					
			_								4.5					
2	120		-10													
2 CS	120		-													
			-11								3.5					
				11.5' sand (0-10%).				E								
		2 (1 )	-12			1		<u>ار ، ا</u> ۱				1				
I hereb Signati	-	y that	the info	ormation on this form is true and cor	Firm Ram	-	cnowled	ige.					- T 1	(11.1)	027.24	07
	ح	-	- >	hr		DOII /. Florida	St., Fif	th Floo	r, Milv	vaukee	, WI 53	204		(414) (414)		

Template: RAMBOLL MINNESOTA BORING LOG - Project: NE_BALDWIN_2024.GPJ



				Boring Number MW-350R							Pag	ge 2	of .	3
Sar	nple									Soil	Prop	erties		
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well Diagram	þ	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
Amn 3 CS 4 CS	Length 150 150 150 150 150 150 150 150 150 150	Blow	13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	<ul> <li>Lach Major Unit</li> <li>0 - 14.4' SILTY CLAY: CL/ML, grayish brown (10YR 5/2), yellowish brown (10YR 5/8) mottling (30-40%), organics material and roots (0-10%), medium to high toughness, low to medium plasticity, moist. <i>(continued)</i></li> <li>14.4 - 24.6' LEAN CLAY: CL, brown (10YR 5/3), light gray (10YR 7/1) mottling (20-30%), yellowish brown (10YR 5/8) mottling (20-30%), sand (20-30%), silt (20-30%), low to medium plasticity, moist.</li> <li>19.7' brown (7.5YR 5/3), sand (0-10%), high plasticity.</li> <li>21.7' - 24.6' coarse subangular gravel (10-20%).</li> <li>24.6 - 26.3' Weathered SHALE Bedrock: BDX (SH), olive gray (5Y 5/2), highly weathered, very weak.</li> <li>26.3 - 27.1' LIMESTONE: BDX (LS), dark gray (10YR 4/1), fresh, competent, fossiliferous, medium bedded, strong.</li> <li>27.1 - 28.3' SHALE: BDX (SH), very dark gray</li> </ul>	CL/ML CL/ML CL BDX (SH) BDX (LS)		Well Diagree		3.5 3.5 1.5 1.5 3 3 2	Moist	Liquic	Plasti	P 200	RQD/
			-28 -29 -30 -31 -32	27.1 - 28.3' <b>SHALE:</b> BDX (SH), very dark gray (10YR 3/1), medium bedded, very weak to weak, dry. 28.3 - 28.9' <b>LIMESTONE:</b> BDX (LS), dark gray (10YR 4/1), fresh, competent fossiliferous, medium bedded, strong. 28.9 - 32.2' <b>SHALE:</b> BDX (SH), very dark gray (10YR 3/1), lightly to moderately weathered, medium bedded.	BDX (SH) BDX (LS) BDX (SH)									



				Boring Number MW-350R							Pa	ge 3	of	3
Sar	nple									Soil	Prop	erties		
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well Diagram		Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
5 CS	60 60		-33 -34 -35 -36 -37	<ul> <li>32.2 - 39.5' SHALEY LIMESTONE: BDX (LS/SH), reddish gray (2.5YR 5/1), very slightly weathered, strong.</li> <li>34.5' moderately decomposed, laminated.</li> </ul>	BDX (LS/SH									
6 CS	48 48			39.5 - 41.7' <b>SHALE:</b> BDX (SH), gray (10YR 5/1), weathered, laminated, very weak to weak. 41.7 - 47' LIMESTONE: BDX (LS), light gray	BDX (SH)			- 						
7 CS	36 36		42 43 44 45 46	41.7 - 47' LIMESTONE: BDX (LS), light gray (10YR 7/1), laminated, medium bedded, strong.	BDX (LS)									

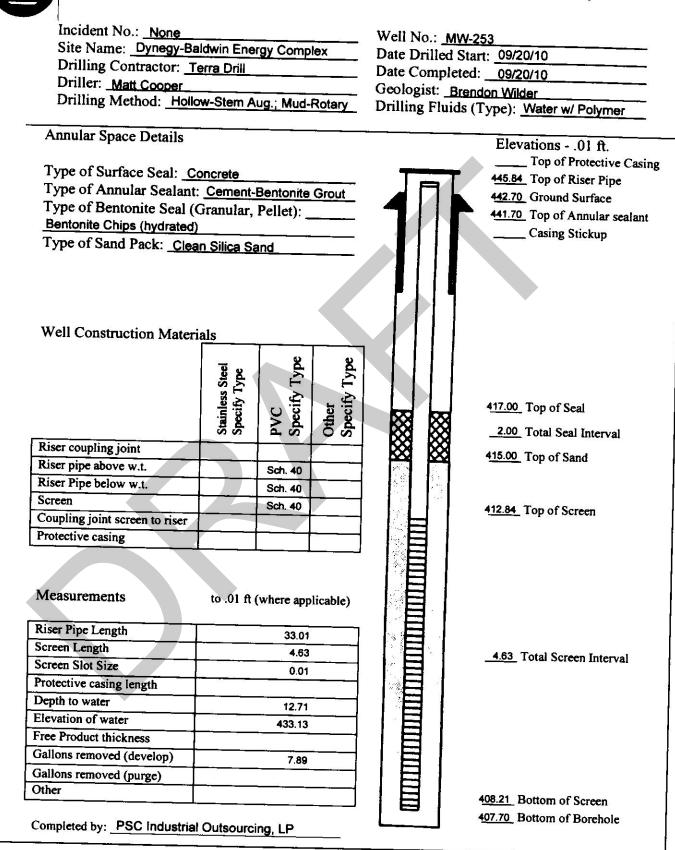
Illinois Environmen	ntal Protection Agency	W	ell Completion Report
Incident No.: <u>None</u>		Well No.: <u>MW</u>	-150
Site Name: Dynegy-Bald		Date Drilled St	art: 09/08/10
Drilling Contractor: <u>Te</u>	rra Drill	Date Complete	
Driller: Matt Cooper		Geologist: <u>Bre</u>	ndon Wilder
Drilling Method: Hollow	v-Stem Auger	Drilling Fluids	(Type): None
Annular Space Details			Elevations01 ft.
Type of Surface Seal: <u>Co</u>	ncrete		396.54 Top of Riser Pipe
Type of Annular Sealant:	Bentonite Chips		393.84 Ground Surface
Type of Bentonite Seal (G			392.84 Top of Annular sealant
Bentonite Chips (hydrated)			Casing Stickup
Type of Sand Pack: Clear	n Silica Sand		
Well Construction Materia	als		
	ب به		
	yp Pe ee		
	S SS L		
	Stainless Steel Specify Type Specify Typ Other Specify Typ		383.34 Top of Seal
	Stainless Steel Specify Type PVC Specify Type Other Specify Type		3.00 Total Seal Interval
Riser coupling joint			380.34 Top of Sand
Riser pipe above w.t.	Sch. 40		top of Sand
Riser Pipe below w.t.	Sch. 40	1.2712 - 144 2.772 - 12702	
Screen	Sch. 40		378.82 Top of Screen
Coupling joint screen to riser			stop of Scient
Protective casing			
Massuraments	$t_0 = 01 \oplus (whom om limit)$		
Measurements	to .01 ft (where applicable)		
Riser Pipe Length	17.72		
Riser Pipe Length Screen Length	17.72 9.64		<u>9.25</u> Total Screen Intervai
Riser Pipe Length Screen Length Screen Slot Size	17.72		<u>9.25</u> Total Screen Interval
Riser Pipe Length Screen Length Screen Slot Size Protective casing length	17.72 9.64 0.01		<u>9.25</u> Total Screen Interval
Riser Pipe Length Screen Length Screen Slot Size Protective casing length Depth to water	17.72 9.64 0.01 19.58		<u>9.25</u> Total Screen Intervai
Riser Pipe Length         Screen Length         Screen Slot Size         Protective casing length         Depth to water         Elevation of water	17.72 9.64 0.01		<u>9.25</u> Total Screen Interval
Riser Pipe Length Screen Length Screen Slot Size Protective casing length Depth to water Elevation of water Free Product thickness	17.72 9.64 0.01 19.58 376.96		<u>9.25</u> Total Screen Interval
Riser Pipe LengthScreen LengthScreen Slot SizeProtective casing lengthDepth to waterElevation of waterFree Product thicknessGallons removed (develop)	17.72 9.64 0.01 19.58		<u>9.25</u> Total Screen Intervai
Riser Pipe LengthScreen LengthScreen Slot SizeProtective casing lengthDepth to waterElevation of waterFree Product thickness	17.72 9.64 0.01 19.58 376.96		<u>9.25</u> Total Screen Interval 369.18 Bottom of Screen

Illinois Environm	ental Protection Agency	v	ell Completion Report
Incident No.: None		Well No.: <u>MW</u>	-152
Site Name: Dynegy-Ba		Date Drilled St	
Drilling Contractor: <u>T</u>	erra Drill	Date Complete	d: 09/23/10
Driller: <u>Matt Cooper</u>		Geologist: Bre	ndon Wilder
Drilling Method: <u>Holk</u>	ow-Stem Auger	Drilling Fluids	(Type): None
Annular Space Details			Elevations01 ft.
<b>T</b>			Top of Protective
Type of Surface Seal: <u>C</u>			424.99 Top of Riser Pipe
Type of Annular Sealant			422.18 Ground Surface
Type of Bentonite Seal (	Granular, Pellet):		4 <u>21.18</u> Top of Annular se
Bentonite Chips (hydrated)			Casing Stickup
Type of Sand Pack: <u>Clea</u>	an Silica Sand		
Well Construction Mater	iala.		
wen construction water			
	be be a		
	T Ty Ste		
	less ify ify ify		418.68 Top of Seal
	Stainless Steel Specify Type PVC Specify Type Other Specify Type		
	S S S S S S S S S S S S S S S S S S S		2.00 Total Seal Interval
Riser coupling joint			416.68 Top of Sand
Riser pipe above w.t. Riser Pipe below w.t.	Sch. 40		
Screen	Sch. 40		
Coupling joint screen to riser	Sch. 40		415.11 Top of Screen
Protective casing			
. Toteen ve cusing			
1 locolive cusing			
Measurements	to .01 ft (where applicable)		
Measurements			
Measurements Riser Pipe Length	9.88		
Measurements Riser Pipe Length Screen Length	9.88 9.25		<u>9.64</u> Total Screen Interv
Measurements           Riser Pipe Length           Screen Length           Screen Slot Size	9.88		<u>9.64</u> Total Screen Interv
Measurements          Riser Pipe Length         Screen Length         Screen Slot Size         Protective casing length	9.88 9.25 0.01		<u>9.64</u> Total Screen Interv
Measurements           Riser Pipe Length           Screen Length           Screen Slot Size	9.88 9.25 0.01 7.35		<u>9.64</u> Total Screen Interv
Measurements          Riser Pipe Length         Screen Length         Screen Slot Size         Protective casing length         Depth to water         Elevation of water	9.88 9.25 0.01		<u>9.64</u> Total Screen Interv
Measurements          Riser Pipe Length         Screen Length         Screen Slot Size         Protective casing length         Depth to water         Elevation of water         Free Product thickness	9.88 9.25 0.01 7.35 417.64		<u>9.64</u> Total Screen Interv
Measurements Riser Pipe Length Screen Length Screen Slot Size Protective casing length Depth to water Elevation of water Free Product thickness Gallons removed (develop)	9.88 9.25 0.01 7.35		<u>9.64</u> Total Screen Interv
Measurements          Riser Pipe Length         Screen Length         Screen Slot Size         Protective casing length         Depth to water         Elevation of water         Free Product thickness	9.88 9.25 0.01 7.35 417.64		<u>9.64</u> Total Screen Interv 405.47 Bottom of Screen

Illinois Environm	ental Protection Agency	V	Vell Completion Repor
Incident No.: <u>None</u>		Well No.: <u>MW</u>	1.252
Site Name: Dynegy-Ba	aldwin Energy Complex	Date Drilled S	
Drilling Contractor: _T		Date Complete	
Driller: Matt Cooper		Geologist: Bre	va. <u>V9/22/10</u>
	ow-Stem Aug.; Mud-Rotary	Drilling Fluids	(Type): <u>Water w/ Polyn</u>
Annular Space Details		·	Elevations01 ft.
			Top of Protecti
Type of Surface Seal: <u>C</u>	oncrete		425.07 Top of Riser Pi
Type of Annular Sealant	: Cement-Bentonite Grout		422.27 Ground Surface
Type of Bentonite Seal (	Granular, Pellet):		421.27 Top of Annula
Bentonite Chips (hydrated			Casing Stickup
Type of Sand Pack: <u>Clea</u>	an Silica Sand		
			~
Well Construction Mater	ials		
	Type Type		
	ecify T ecify T rer		382.97 Top of Seal
	Stainless Specify T PVC Specify Other Specify		1.5
Riser coupling joint	Stainless Steel Specify Type PVC Specify Type Other Specify Type		3.70 Total Seal Inter
Riser coupling joint Riser pipe above w.t.			0.0
	Sch. 40		3.70 Total Seal Inter
Riser pipe above w.t.	Sch. 40 Sch. 40		<u>3.70</u> Total Seal Inter <u>379.27</u> Top of Sand
Riser pipe above w.t. Riser Pipe below w.t.	Sch. 40		3.70 Total Seal Inter
Riser pipe above w.t. Riser Pipe below w.t. Screen	Sch. 40 Sch. 40		<u>3.70</u> Total Seal Inter <u>379.27</u> Top of Sand
Riser pipe above w.t. Riser Pipe below w.t. Screen Coupling joint screen to riser	Sch. 40 Sch. 40		<u>3.70</u> Total Seal Inter <u>379.27</u> Top of Sand
Riser pipe above w.t. Riser Pipe below w.t. Screen Coupling joint screen to riser	Sch. 40 Sch. 40		<u>3.70</u> Total Seal Inter <u>379.27</u> Top of Sand
Riser pipe above w.t. Riser Pipe below w.t. Screen Coupling joint screen to riser Protective casing	Sch. 40           Sch. 40           Sch. 40           Sch. 40		<u>3.70</u> Total Seal Inter <u>379.27</u> Top of Sand
Riser pipe above w.t. Riser Pipe below w.t. Screen Coupling joint screen to riser Protective casing	Sch. 40 Sch. 40		<u>3.70</u> Total Seal Inter <u>379.27</u> Top of Sand
Riser pipe above w.t. Riser Pipe below w.t. Screen Coupling joint screen to riser Protective casing Measurements	to .01 ft (where applicable)		<u>3.70</u> Total Seal Inter 379.27 Top of Sand
Riser pipe above w.t. Riser Pipe below w.t. Screen Coupling joint screen to riser Protective casing Measurements Riser Pipe Length	Sch. 40           Sch. 40           Sch. 40           Sch. 40           to .01 ft (where applicable)           47.21		<u>3.70</u> Total Seal Inter 379.27 Top of Sand 377.87 Top of Screen
Riser pipe above w.t. Riser Pipe below w.t. Screen Coupling joint screen to riser Protective casing Measurements Riser Pipe Length Screen Length	Sch. 40           Sch. 40           Sch. 40           Sch. 40           Image: scheme structure           to .01 ft (where applicable)           47.21           4.63		<u>3.70</u> Total Seal Inter 379.27 Top of Sand 377.87 Top of Screen
Riser pipe above w.t. Riser Pipe below w.t. Screen Coupling joint screen to riser Protective casing Measurements Riser Pipe Length Screen Length Screen Slot Size	Sch. 40           Sch. 40           Sch. 40           Sch. 40           to .01 ft (where applicable)           47.21		<u>3.70</u> Total Seal Inter 379.27 Top of Sand 377.87 Top of Screen
Riser pipe above w.t. Riser Pipe below w.t. Screen Coupling joint screen to riser Protective casing Measurements Riser Pipe Length Screen Length Screen Slot Size Protective casing length	Sch. 40           Sch. 40           Sch. 40           Sch. 40           Image: scheme structure           to .01 ft (where applicable)           47.21           4.63           0.01		<u>3.70</u> Total Seal Inter 379.27 Top of Sand 377.87 Top of Screen
Riser pipe above w.t. Riser Pipe below w.t. Screen Coupling joint screen to riser Protective casing Measurements Riser Pipe Length Screen Length Screen Slot Size Protective casing length Depth to water	Sch. 40           Sch. 40           Sch. 40           Sch. 40           Image: scheme structure           to .01 ft (where applicable)           47.21           4.63           0.01		<u>3.70</u> Total Seal Inter 379.27 Top of Sand 377.87 Top of Screen
Riser pipe above w.t. Riser Pipe below w.t. Screen Coupling joint screen to riser Protective casing Measurements Riser Pipe Length Screen Length Screen Slot Size Protective casing length Depth to water Elevation of water	Sch. 40           Sch. 40           Sch. 40           Sch. 40           Image: scheme structure           to .01 ft (where applicable)           47.21           4.63           0.01		<u>3.70</u> Total Seal Inter 379.27 Top of Sand 377.87 Top of Screen
Riser pipe above w.t. Riser Pipe below w.t. Screen Coupling joint screen to riser Protective casing Measurements Riser Pipe Length Screen Length Screen Length Screen Slot Size Protective casing length Depth to water Elevation of water Free Product thickness	Sch. 40           Sch. 40           Sch. 40           Sch. 40           Image: scheme structure           to .01 ft (where applicable)           47.21           4.63           0.01           0.40           424.67		<u>3.70</u> Total Seal Inter 379.27 Top of Sand 3 <u>77.87</u> Top of Screen
Riser pipe above w.t. Riser Pipe below w.t. Screen Coupling joint screen to riser Protective casing Measurements Riser Pipe Length Screen Length Screen Slot Size Protective casing length Depth to water Elevation of water Free Product thickness Gallons removed (develop)	Sch. 40           Sch. 40           Sch. 40           Sch. 40           Image: scheme structure           to .01 ft (where applicable)           47.21           4.63           0.01		<u>3.70</u> Total Seal Inter 379.27 Top of Sand 3 <u>77.87</u> Top of Screen
Riser pipe above w.t. Riser Pipe below w.t. Screen Coupling joint screen to riser Protective casing Measurements Riser Pipe Length Screen Length Screen Length Screen Slot Size Protective casing length Depth to water Elevation of water Free Product thickness	Sch. 40           Sch. 40           Sch. 40           Sch. 40           Image: sch and scheme state scheme		<u>3.70</u> Total Seal Inter <u>379.27</u> Top of Sand

## Illinois Environmental Protection Agency

Well Completion Report



# Illinois Environmental Protection Agency

Well Completion Report

Incident No.: <u>None</u> Site Name: Dynegy-Bal	dwin Energy Comple		Well No.: <u>MW</u> Date Drilled S	
Drilling Contractor: Te			Date Complete	
Driller: Matt Cooper			Geologist: Bre	
Drilling Method: Hollo	w-Stem Aug.; Mud-F	Rotary		(Type): <u>Water w/ Polymer</u>
Annular Space Details	<u></u>		2000 <b>-</b>	Elevations01 ft.
Type of Surface Seal: _Co	norete			Top of Protective Casi
Type of Annular Sealant:		Grout	Jeil	3 <u>96.80</u> Top of Riser Pipe 3 <u>94.11</u> Ground Surface
Type of Bentonite Seal (				
Bentonite Chips (hydrated)		<u> </u>		<u>393.11</u> Top of Annular sealan
Type of Sand Pack: <u>Clea</u>				Casing Stickup
- ) <u></u>				
Well Construction Materi	ials			
	Stainless Steel Specify Type PVC Specify Type	Other Specify Type		3 <u>67.71</u> Top of Seal 10.60 Total Seal Interval
Riser coupling joint				
Riser pipe above w.t.	Sch. 40			3 <u>57.11</u> Top of Sand
Riser Pipe below w.t.	Sch. 40			
Screen	Sch. 40			352.52 Top of Screen
Coupling joint screen to riser				rop or beredit
Protective casing		·		
Measurements Riser Pipe Length	to .01 ft (where app 44.25			
Screen Length	4.63			4.63 Total Screen Interval
Screen Slot Size	0.01			
Protective casing length	5.01			
Depth to water	22.52			
Elevation of water	374.28			
Free Product thickness				
Gallons removed (develop)	10.00	)		
	1			
Gallons removed (purge)				
				347.89 Bottom of Screen

#### Illinois Environmental Protection Agency Well Completion Report Incident No.: None Well No.: MW-352 Site Name: Dynegy-Baldwin Energy Complex Date Drilled Start: 09/15/10 Drilling Contractor: Terra Drill Date Completed: __09/17/10 Driller: Matt Cooper Geologist: Brendon Wilder Drilling Method: Hollow-Stem Aug.; Mud-Rotary Drilling Fluids (Type): Water w/ Polymer Annular Space Details Elevations - .01 ft. Top of Protective Casing Type of Surface Seal: Concrete 425.04 Top of Riser Pipe Type of Annular Sealant: Cement-Bentonite Grout 422.38 Ground Surface Type of Bentonite Seal (Granular, Pellet): 421.36 Top of Annular sealant Bentonite Chips (hydrated) Casing Stickup Type of Sand Pack: Clean Silica Sand Well Construction Materials Type Stainless Steel Specify Type Specify Type Other Specify 361.06 Top of Seal PVC 4.00 Total Seal Interval Riser coupling joint 357.06 Top of Sand Riser pipe above w.t. Sch. 40 Riser Pipe below w.t. Sch. 40 Screen Sch. 40 354.46 Top of Screen Coupling joint screen to riser Protective casing Measurements to .01 ft (where applicable) **Riser Pipe Length** 70.59 Screen Length 4.63 4.63 Total Screen Interval Screen Slot Size 0.01 Protective casing length Depth to water 23.85 Elevation of water 401.19 Free Product thickness Gallons removed (develop) 13.70 Gallons removed (purge) Other 349.83 Bottom of Screen 348.56 Bottom of Borehole Completed by: PSC Industrial Outsourcing, LP



Facility/Project Name	Local Grid Location of Well		Well Name
Baldwin Energy Complex	t. □ N. Local Grid Origin □ (estimated: □ ) o	$_ft. \square W.$	
Facility License, Permit or Monitoring No.			
	Lat. <u>38°</u> <u>11'</u> <u>31.888"</u> Long. <u>-89</u>	$\frac{9^{\circ}}{20.441''}$ or	MW-366
Facility ID	St. Plane555,581.80 ft. N,2,381,17	1.15 ft. E. E/Ŵ	Date Well Installed
	Section Location of Waste/Source	<u>0</u>	12/04/2015
Type of Well	1/4 of 1/4 of Sec, T	NR DW	Well Installed By: (Person's Name and Firm)
mw	Location of Well Relative to Waste/Source	Gov. Lot Number	Jim Dittmaier
Distance from Waste/ State	u 🗆 Upgradient 🥼 s 🗆 Sidegradie		
tt. Illinois	d 🛛 Downgradient 🛛 n 🗆 Not Know		
A. Protective pipe, top elevation	ft. (NAVD <del>88)</del> •	1. Cap and lock?	🛛 Yes 🗆 No
B. Well casing, top elevation 42	25.08 ft. (NAVD88)	2. Protective cover p a. Inside diameter	
C. Land surface elevation 42	22.54 ft. (NAVD88)	b. Length:	<u>5.0</u> ft.
D. Surface seal, bottom <u>421.5</u> ft. (NAV		c. Material:	Steel 🛛 Other 🗆
12. USCS classification of soil near screen:		d. Additional prote	
		If yes, describe	
	ССНС		Bentonite
Bedrock 🛛		3. Surface seal:	Concrete 🛛
13. Sieve analysis attached? $\Box$ Ye	es 🖾 No	X	Other
14. Drilling method used: Rotar	y 🖂 🛛 👹 👹	4. Material between	well casing and protective pipe:
Hollow Stem Aug	er 🗆 🛛 👹 👹		Bentonite 🖂
Oth	er 🗆 🛛 📓 📓		Sand Other 🛛
	🛛 🗮 👹 🗕		l: a. Granular/Chipped Bentonite
6			nud weight Bentonite-sand slurry $\Box$
Drilling Mud D 0 3 Nor			ud weight Bentonite slurry □
16. Drilling additives used? $\Box$ Ye	es 🛛 No	d. <u>30</u> % Bentom	
	ir □ le □ es ⊠ No	eFt f. How installed:	volume added for any of the above Tremie $\Box$
Describe		1. How instance.	Tremie pumped
17. Source of water (attach analysis, if required	):		Gravity
Village of Baldwin		6. Bentonite seal:	a. Bentonite granules
		/	$3/8$ in. $\Box$ 1/2 in. Bentonite chips $\boxtimes$
E. Bentonite seal, top ft. (NAV	(D88) or 35.0 ft		Other
_		7. Fine sand material	l: Manufacturer, product name & mesh size
F. Fine sand, top ft. (NAV	D88).orft.	a b. Volume added	ft ³
G. Filter pack, top <u>382.5</u> ft. (NAV	D88) or 40.0 ft.		al: Manufacturer, product name & mesh size
		/ •	nin Corporation, FILTERSIL
H. Screen joint, top 380.5 ft. (NAV	D88) or 42.0 ft.	b. Volume added	ft ³
		9. Well casing:	Flush threaded PVC schedule 40
I. Well bottom $370.5$ ft. (NAV	D88) or 52.0 ft.		Flush threaded PVC schedule 80 $\Box$
270.0	D88).or 52.5 ft.		Other
J. Filter pack, bottom $370.0$ ft. (NAV	D88) or 52.5 ft.	> 10. Screen material:	Schedule 40 PVC
268.5	540	a. Screen Type:	Factory cut
K. Borehole, bottom ft. (NAV	D88) or 54.0 ft.		Continuous slot
60		h. Manafastana	Other
L. Borehole, diameter $6.0$ in.		b. Manufacturer c. Slot size:	0.010 in.
M. O.D. well casing $2.38$ in.		d. Slotted length:	<u></u>
$\frac{1}{100} \text{ mm} = \frac{1}{100} \text{ mm}.$	Ň	11. Backfill material (	
N. I.D. well casing <u>2.07</u> in.			$\frac{drock drill cuttings}{drock drill cuttings}$
····			
I hereby certify that the information on this form	n is true and correct to the best of my knowled	ge.	Date Modified: 2/4/2016
Signature 2 M /	Firm Natural Resource		Tel: (414) 837-3607

Signature	Brad Rucher	234 W. Florida Street, Floor 5, Milwaukee, WI 53204	Fax: (414) 837-3607



Facility/Project Name	Local Grid Location of Well			Well Name	
Baldwin Energy Complex	$= \underbrace{ft.}_{S.}  =$	ft.	$\square$ E. $\square$ W.		
Facility License, Permit or Monitoring No.					
	Lat. <u>38°</u> <u>11'</u> <u>30.440''</u>	Long. <u>-89°</u>		MW-384	
Facility ID	St. Plane555,446.11 ft. N,	2,384,518.72	_ ft. E. E / 🕅	Date Well Installed	
	Section Location of Waste/Source	ce		12/18/2015	
Type of Well	1/4 of 1/4 of Sec.	, T	N, R. $\square W$	Well Installed By: (Person's Name ar	id Firm)
mw           Distance from Waste/         State		loter boulee	Gov. Lot Number	Chad Dutton	
Source		Sidegradient		Bulldog Drilling	
t Development In the second se	d ⊠ Downgradient n □		L — — — — — — — — — — — — — — — — — — —	∠ Dundog Drinnig	
	ft. (NAVD <del>88)</del>		2. Protective cover pi		
B. Well casing, top elevation 45	58.95 ft. (NAVD88)		a. Inside diameter:	-	<u>4.0</u> in.
C. Land surface elevation4	66.70 ft. (NAVD88)		b. Length:	=	<u>5.0</u> ft.
		15.125.12	c. Material:	Steel	$\boxtimes$
D. Surface seal, bottom ft. (NAV	/D88)_or ^{1.0} ft.	1959		Other	
12. USCS classification of soil near screen:			d. Additional prote	ection?	
	V C SP C CH		If yes, describe.	teel bollards (3), 6" PVC casing to 25'	
$ SM \square SC \square ML \square MH \square Cl Bedrock \boxtimes $			3. Surface seal:	Bentonite	_
13. Sieve analysis attached? $\Box$ Ye	rs ⊠ No			Concrete	
			1 Material between y	well casing and protective pipe:	
14. Drilling method used: Rotar Hollow Stem Aug	- 88		+. Material between v	Bentonite	$\boxtimes$
	er 🗆 🛛 🕷			Sand Other	
			5 Annular space seal	a. Granular/Chipped Bentonite	
15. Drilling fluid used: Water $\boxtimes 02$ A	ir □ e □ es ⊠ No			ud weight Bentonite-sand slurry	
Drilling Mud 0 3 Nor	e 🗆 🛛 👹			ud weight Bentonite slurry	
			d. <u>30</u> % Benton	ite Bentonite-cement grout	
16. Drilling additives used? $\Box$ Ye	es ⊠ No		eFt ³	volume added for any of the above	
			f. How installed:	Tremie	
Describe 17. Source of water (attach analysis, if required				Tremie pumped	$\boxtimes$
17. Source of water (attach analysis, if required	):			Gravity	
Village of Baldwin			6. Bentonite seal:	a. Bentonite granules	
				$3/8$ in. $\Box 1/2$ in. Bentonite chips	
E. Bentonite seal, top $402.7$ ft. (NAV	D88) or 54.0 ft.			Other	
			7. Fine sand material	: Manufacturer, product name & mesh	i size
F. Fine sand, top ft. (NAV	D88 <u>) or</u> ft.		a	ft ³	
C Eiter rest to $398.2$ $C$ (MAX)	D88) or 58.5 ft.		b. Volume added		h size
G. Filter pack, top <u>398.2</u> ft. (NAV	Doo <u>) of 50.5</u> II.		- Linia	nin Corporation, FILTERSIL	SII SIZC
H. Screen joint, top <u>396.2</u> ft. (NAV	D88) or 60.5 ft.		a. <u>Unin</u> b. Volume added	ft ³	_
		- / ,	9. Well casing:	Flush threaded PVC schedule 40	$\boxtimes$
I. Well bottom 386.2 ft. (NAV	D88) or 70.5 ft.		, wen easing.	Flush threaded PVC schedule 80	
				Other	
J. Filter pack, bottom 385.2 ft. (NAV	D88) or 71.5 ft.		0. Screen material:	Schedule 40 PVC	
			a. Screen Type:	Factory cut	$\boxtimes$
K. Borehole, bottom ft. (NAV	D88) or 77.0 ft.			Continuous slot	
				Other	
L. Borehole, diameter $6.0$ in.			b. Manufacturer		0.010
2.20		$\langle \rangle$	c. Slot size:		$\frac{0.010}{10.0}$ in.
M. O.D. well casing $2.38$ in.			<ul><li>d. Slotted length:</li><li>1. Backfill material (1)</li></ul>	halow filter past:	<u>10.0</u> ft.
N. I.D. well casing 2.07 in.		1.	0.5' of bentonite chi	below filter pack): None ps, 5' of bedrock drill cuttings Other	
N. I.D. well casing $2.07$ in.					<u>2</u> 3
I hereby certify that the information on this form	is true and correct to the best of	my knowledge		Date Modified: 2/4/2016	
	<b>D</b> '	Resource Tech	nology	Tel: (414) 837-3607	
Signature Brad Rucher	Tuturur		5, Milwaukee, WI 5		



Facility/Project Name	Local Grid Location of W	ell		Well Name	
Baldwin Energy Complex		ft.	$\square$ E. $\square$ W.		
Facility License, Permit or Monitoring No.	Local Grid Origin 🔲 (	estimated:  ) or W	Vell Location		
	Lat. <u>38° 11' 22.</u>	<u>855''</u> Long. <u>-89°</u>		PZ-174	
Facility ID	St. Plane554,666.23		_ ft. E. E / 🛞	Date Well Installed	
True of Wall	Section Location of Waste	e/Source		08/04/2015	- 1 Finne)
Type of Well	1/4 of 1/4 of	of Sec, T	N, R. $\square W$	Well Installed By: (Person's Name a	nd Firm)
Distance from Waste/ State	Location of Well Relative	to Waste/Source	Gov. Lot Number	Chad Dutton	
Source	u 🗆 Upgradient	s 🗆 Sidegradient		Bulldog Drilling	
	d 🖾 Downgradient		. Cap and lock?	<u> </u>	□ No
	ft. (NAVD <del>88)</del>		2. Protective cover pi		
B. Well casing, top elevation 40	1.92 ft. (NAVD88)		a. Inside diameter:		<u>4.0</u> in.
C. Land surface elevation 39	<u>8.97</u> ft. (NAVD88)		b. Length:	_	<u>5.0</u> ft.
		15.55.5	c. Material:	Steel	$\boxtimes$
D. Surface seal, bottom <u>398.0</u> ft. (NAV	/D88)_off.0_ ft.			Other	
12. USCS classification of soil near screen:			d. Additional prote		🗆 No
	$V \Box SP \Box $		If yes, describe:		
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	CH 🗆		Surface seal:	Bentonite	
13. Sieve analysis attached?	s 🖾 No			Concrete Other	
14. Drilling method used: Rotar			Material between y	well casing and protective pipe:	
Hollow Stem Aug	5		F. Iviaterial Detween v	Bentonite	
	ar 🗆			Sand Other	
			Annular space sea	l: a. Granular/Chipped Bentonite	
15. Drilling fluid used: Water ⊠ 0 2 A	ir 🗆 🛛			ud weight Bentonite-sand slurry	
Drilling Mud 0 3 Nor	e 🗆		c. Lbs/gal m	ud weight Bentonite suite suitery	
			d% Benton	ite Bentonite-cement grout	
16. Drilling additives used? $\Box$ Ye	s 🖾 No			volume added for any of the above	_
			f. How installed:		$\boxtimes$
Describe				Tremie pumped	
17. Source of water (attach analysis, if required	l):			Gravity	
Village of Baldwin		6	6. Bentonite seal:	a. Bentonite granules	
				$3/8$ in. $\Box 1/2$ in. Bentonite chips	
E. Bentonite seal, top ft. (NAV	D88) or 1.0 ft.			Other	
			7. Fine sand material	: Manufacturer, product name & mes	sh size
F. Fine sand, top ft. (NAV	D8 <u>8) or</u> ft.		a	. 2	
2965 0 0141	125 0	KY KY /	b. Volume added		, ·
G. Filter pack, top <u>386.5</u> ft. (NAV	D88 <u>) or 12.5</u> ft.		•	I: Manufacturer, product name & me	sh size
384.5 0 0141	D00) 145 0		u	nin Corporation, FILTERSIL	
H. Screen joint, top <u>384.5</u> ft. (NAV	D88) or 14.5 ft.		b. Volume added		
L Well bettern 374.5. # (NAX)	D88) or 24.5 ft.		. Well casing:	Flush threaded PVC schedule 40	
I. Well bottom $3/4.5$ ft. (NAV	D88) 01 2 1.5 II.			Flush threaded PVC schedule 80	
J. Filter pack, bottom ft. (NAV	D88) or 24.5 ft.		). Screen material:	Schedule 40 PVC Other	
J. Filter pack, bottom			a. Screen Type:	Factory cut	
K. Borehole, bottom 374.5 ft. (NAV	D8 <u>8) or 24.5</u> ft. <		a. Sereen Type.	Continuous slot	
				Other	
L. Borehole, diameter <u>8.3</u> in.			b. Manufacturer	Outer	
		$\backslash$	c. Slot size:		0.010 in.
M. O.D. well casing $2.38$ in.		$\backslash$	d. Slotted length:	_	<u>10.0</u> ft.
		× 11	. Backfill material (	below filter pack): None	
N. I.D. well casing $2.07$ in.				Other	
-					
I hereby certify that the information on this form		best of my knowledge.		Date Modified: 11/6/2015	
Signature	Firm Nat	tural Resource Techi	nology	Tel: (414) 837-3607	
Jahn M. Hufl	234	W. Florida Street, Floor	5, Milwaukee, WI 5	Fax: (414) 837-3608	



Facility/Project Name	Local Grid Loca	tion of Well			Well Name	
Baldwin Energy Complex		_ft. □ S. –	ft.	□ E. □ W. Well Location ⊠		
Facility License, Permit or Monitoring No.						
	-			<u>52'</u> <u>17.843"</u> or	PZ-176	
Facility ID	St. Plane554	<u>,264.76</u> ft. N	J, <u>2,381,381.02</u>	ft. EE/ 🕅	Date Well Installed	
Type of Well	Section Location	n of Waste/Sour	rce	ПБ	08/06/2015 Well Installed By: (Person's Name a	and Firm)
Type of wen	1/4 of	1/4 of Sec	2, T	N, R. $\square \overset{\square}{=} \overset{\mathbb{B}}{W}$		and Firm)
Distance from Waste/ State	Location of Well	l Relative to W	aste/Source	Gov. Lot Number	Chad Dutton	
Source	u 🗆 Upgradi		□ Sidegradient		Bulldog Drilling	
	d ⊠ Downgr ft. (NAVE			1. Cap and lock?		s 🗆 No
				2. Protective cover p		5 🖾 100
B. Well casing, top elevation 40	06.44 ft. (NAVE	)88)	H	a. Inside diameter		<u>4.0</u> in.
C. Land surface elevation 40	03.46 ft. (NAVE	(88)		b. Length:		5.0 ft.
D. Surface seal, bottom402.5_ft. (NA*			15.25.21	c. Material:	Steel	
	<u>vD88j0⊧.</u> II.	1.216.216.2			Other	
12. USCS classification of soil near screen:		OVIC OVIC OVIC	A A A A A A A A A A A A A A A A A A A	d. Additional prote		s 🗆 No
	$\begin{array}{c c} W \square & SP \square \\ L \boxtimes & CH \square \end{array}$			If yes, describe:		_
Bedrock		X		3. Surface seal:	Bentonite Concrete	
13. Sieve analysis attached? $\Box$ Ye	es 🛛 No	×			Other	
	ry 🗆	×		4 Material between	well casing and protective pipe:	
Hollow Stem Aug	5	×			Bentonite	$\simeq$
	er 🗆	×	\$ ₿		Sand Other	
			å 🗱 —	5. Annular space sea	l: a. Granular/Chipped Bentonite	• <b>□</b>
15. Drilling fluid used: Water ⊠ 0 2 A	Air 🗆			bLbs/gal m	ud weight Bentonite-sand slurry	<i>r</i> 🗌
Drilling Mud 0 3 Nor	ne 🗆			cLbs/gal m	ud weight Bentonite slurry	/
				d. <u>30</u> % Benton	ite Bentonite-cement grout	í 🛛
16. Drilling additives used?	es 🖾 INO			eFt ³	volume added for any of the above	
Describe				f. How installed:		
17. Source of water (attach analysis, if required			3 🕅		Tremie pumped	
	u).		8 🕅		Gravity	
Village of Baldwin			8 🛞 🖉	6. Bentonite seal:	a. Bentonite granules	
202.5	11.0				$3/8$ in. $\Box 1/2$ in. Bentonite chips	
E. Bentonite seal, top ft. (NAV	VD88 <u>) or 11.0</u> f	t.	▌▓ / .		Other	
	(00)	, \ 🕷	8 🕅 / /		l: Manufacturer, product name & me	sh size
F. Fine sand, top ft. (NAV	(D88) or 1	ì. 🔪 🔪	\$ ₿/ /	a b. Volume added	ft ³	
G. Filter pack, top <u>387.5</u> ft. (NAV	VD88 <u>) or 16.0</u> f	, <b>∖</b> [	3 🖾 / ,		al: Manufacturer, product name & m	resh size
	1000)01 1			-	nin Corporation, FILTERSIL	Con Size
H. Screen joint, top <u>385.4</u> ft. (NAV	/D88) or 18.1 f	1		b. Volume added		
	1.200,000 1			9. Well casing:	Flush threaded PVC schedule 40	
I. Well bottom 375.4 ft. (NAV	VD88) or 28.1 f	t. 🔪 🛛		0	Flush threaded PVC schedule 80	
					Other	
J. Filter pack, bottom ft. (NAV	/D88) or 28.6 f	t. —		0. Screen material:	Schedule 40 PVC	_
				a. Screen Type:	Factory cut	ί 🛛
K. Borehole, bottom ft. (NAV	/D88) or 28.6 f	ì.			Continuous slot	i 🗆
					Other	: 🗆
L. Borehole, diameter $8.3$ in.						0.010
2.20			$\backslash$	c. Slot size:	-	0.010 in. 10.0 ft.
M. O.D. well casing $2.38$ in.				d. Slotted length:		
N L D III · · · · · · · · · · · · · · · · ·			. 11	1. Backfill material (	below filter pack): None Other	
N. I.D. well casing $2.07$ in.						
I hereby certify that the information on this form	m is true and corr	ect to the best	of my knowledge		Date Modified: 11/6/2015	
Cionotuno		•	Resource Tech	nology	Tel: (414) 837-3607	
Valm M. Hufl		Inatural		r 5, Milwaukee, WI 5		
4						

# RAMBOLL

Facility/Project Name	Local Grid Location of Well			Well Name	
Baldwin Power Plant	Local Grid Origin (estimate	ft.	$\square$ W.		
Facility License, Permit or Monitoring No.	Local Grid Origin (estimate	ed: 🗌 ) or W	Vell Location	MUV 252D	
Facility ID	_Lat '' I			MW-253R Date Well Installed	
Facinity ID	St. Plane ft. N, Section Location of Waste/Source		_ ft. E. E / 🕅		
Type of Well				05/01/2024 Well Installed By: (Person's Name a	nd Firm)
Well Code 12/pz	1/4 of1/4 of Sec	, T	N, R. $\square$ W	Ethan Orange	,
Distance from Waste/ State	Location of Well Relative to Wast     u □ Upgradient s □	Sidegradient	Gov. Lot Number		
Source ft. IL				Cascade Drilling LP	
A. Protective pipe, top elevation	ft. (NAVD <del>88)</del>		. Cap and lock?		🗆 No
B. Well casing, top elevation	ft. (NAVD88)		. Protective cover pi a. Inside diameter:		<u>4.0</u> in.
C. Land surface elevation	ft. (NAVD88)		b. Length:	-	<u>5.0</u> ft.
D. Surface seal, bottom ft. (NA	VD88 <u>) o^{1.0}</u> ft.	15.215.21 16.215.21	c. Material:	Steel Other	
12. USCS classification of soil near screen:	Distriction of the second s	217-217-21 - 215-217-21	d. Additional prote		🗆 No
	W D SP D	$ X \rangle$	If yes, describe:	4 bollards	_
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		3	. Surface seal:	Bentonite Concrete	_
13. Sieve analysis attached?	'es ⊠No			Other	
14. Drilling method used: Rota	ıry 🗆  👹	4	. Material between	well casing and protective pipe:	
Hollow Stem Au				Bentonite	
Sonic Oth	ner 🛛			Other	
		5	. Annular space sea	l: a. Granular/Chipped Bentonite	
15. Drilling fluid used: Water $\boxtimes 0.2$ Drilling Mud $\square 0.3$ No.	Air 🗆	t 🐰 t		ud weight Bentonite-sand slurry	
		KXX		ud weight Bentonite slurry	
16. Drilling additives used?	Yes □ No		1. $5$ % Benton e. $3.5$ $Ft^3$	ite Bentonite-cement grout volume added for any of the above	Ä
N			f. How installed:	-	
Describe <u>N</u>				Tremie pumped	$\boxtimes$
17. Source of water (attach analysis, if require	cd):			Gravity	
Town of Baldwin		6	. Bentonite seal:	a. Bentonite granules	
	22.0			$3/8$ in. $\Box 1/2$ in. Bentonite chips	
E. Bentonite seal, top ft. (NA	VD88)  or  23.0  ft.	8 / 7		. Manufacturer, product name & me	
F. Fine sand, top ft. (NA	VD88).orft.		a	-	
	27.0	.8		ft ³	
G. Filter pack, top ft. (NA	VD88 <u>) or 27.0</u> ft.	8	<ul> <li>Filter pack materia</li> <li>a</li> </ul>	<ul> <li>al: Manufacturer, product name &amp; me #2 K&amp;E Well Gravel</li> </ul>	esh size
H. Screen joint, top ft. (NA	VD88) or 29.5 ft.		b. Volume added	ft ³	_
		9	. Well casing:	Flush threaded PVC schedule 40	
I. Well bottom ft. (NA	VD88 <u>) or 34.5</u> ft.			Flush threaded PVC schedule 80	
			~	Other	
J. Filter pack, bottom ft. (NA	VD88) or 35.0 ft.	∃10	a. Screen material:	Schedule 40 PVC Factory cut	M
K. Borehole, bottom ft. (NA	VD88) or 35.0 ft >		a. Screen Type:	Continuous slot	
				Other	
L. Borehole, diameter <u>6.0</u> in.			b. Manufacturer		
			c. Slot size:	_	$\frac{0.010}{5.0}$ in.
M. O.D. well casing $2.38$ in.		$\backslash$	d. Slotted length:	-	<u>5.0</u> ft.
N. I.D. well casing 2.07 in.		. 11	. Backfill material (	below filter pack): None Other	
N. I.D. well casing $2.07$ in.				Other	
I hereby certify that the information on this for	m is true and correct to the best of r	my knowledge.		Date Modified: 7/9/2024	
Signature	Firm Ramboll	,		Tel: (414) 837-	3607
Ehr		ida St., Fifth Floc	or, Milwaukee, WI 5		

# RAMBOLL

Facility/Project Name	Local Grid Location of Well			Well Name	
Baldwin Power Plant	Local Grid Origin ☐ (estin	ft.	□ E. □ W.		
Facility License, Permit or Monitoring No.	Local Grid Origin (estin	mated: 🗌 ) or V	Vell Location	MUU 250D	
Facility ID	_Lat ''			MW-350R Date Well Installed	
Facinity ID	St. Plane ft. 1 Section Location of Waste/Sou	N,	ft.EE/🛞		
Type of Well				05/03/2024 Well Installed By: (Person's Name a	nd Firm)
Well Code 12/pz	1/4 of1/4 of Se	ю, Т	N, R. $\square$ W	Ethan Orange	,
Distance from Waste/ State	-Location of Well Relative to W u □ Upgradient s	aste/Source	Gov. Lot Number		
Source ft. IL				Cascade Drilling LP	
A. Protective pipe, top elevation	ft. (NAV <del>D88)</del>		1. Cap and lock?		🗆 No
B. Well casing, top elevation	ft. (NAVD88)		<ol> <li>Protective cover pi a. Inside diameter:</li> </ol>		<u>4.0</u> in.
C. Land surface elevation	ft. (NAVD88)		b. Length:	-	<u>5.0</u> ft.
D. Surface seal, bottom ft. (NA	VD88 <u>) or^{1.0}</u> ft.	18.218.21	c. Material:	Steel Other	
12. USCS classification of soil near screen:	Przinizina Dikorzina	215-215-21 - Dis Dis Dis Dis	d. Additional prote		D No
	W 🗆 SP 🗆 🔪 🔪		If yes, describe:	4 bollards	_
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$			3. Surface seal:	Bentonite Concrete	_
13. Sieve analysis attached?	es ⊠ No			Other	
14. Drilling method used: Rota	ry 🗆		4. Material between	well casing and protective pipe:	
Hollow Stem Au				Bentonite	
Sonic Oth	ier 🛛			Other	
		× × · · · ·	5. Annular space sea	l: a. Granular/Chipped Bentonite	
15. Drilling fluid used: Water $\boxtimes 0.2$ Drilling Mud $\square 0.3$ No.	Air 🗆 🛛 🕹			ud weight Bentonite-sand slurry	
	ne 🗆			ud weight Bentonite slurry	
16. Drilling additives used?	es 🗆 No		d. $5$ % Benton e. 4 Ft ³	ite Bentonite-cement grout volume added for any of the above	×
N			f. How installed:		
Describe <u>N</u>		88		Tremie pumped	$\boxtimes$
17. Source of water (attach analysis, if require	d):			Gravity	
Town of Baldwin		× × ×	6. Bentonite seal:	a. Bentonite granules	
	27.0			$3/8$ in. $\Box 1/2$ in. Bentonite chips	
E. Bentonite seal, top ft. (NA	VD88) or 27.0 ft.	8 🛞 / .		Other : Manufacturer, product name & mer	
F. Fine sand, top ft. (NA	VD88).orft.		a	-	
	27.0			ft ³	
G. Filter pack, top ft. (NA	VD88) or 37.0 ft.		<ol> <li>Filter pack materia</li> <li>a</li> </ol>	<ul> <li>al: Manufacturer, product name &amp; me #2 K&amp;E Well Gravel</li> </ul>	esh size
H. Screen joint, top ft. (NA	VD88) or 42.0 ft.		b. Volume added	ft ³	
			9. Well casing:	Flush threaded PVC schedule 40	
I. Well bottom ft. (NA	VD88) or 47.0 ft.			Flush threaded PVC schedule 80	
			~	Other	
J. Filter pack, bottom ft. (NA	VD88) or 47.0 ft.		<ol> <li>Screen material: a. Screen Type:</li> </ol>	Schedule 40 PVC Factory cut	-
K. Borehole, bottom ft. (NA	VD88) or 47.0 ft >		a. Screen Type.	Continuous slot	
				Other	
L. Borehole, diameter <u>6.0</u> in.			b. Manufacturer		
		$\backslash$	c. Slot size:	_	$\frac{0.010}{5.0}$ in.
M. O.D. well casing $2.38$ in.			d. Slotted length:	-	<u>5.0</u> ft.
N. I.D. well casing 2.07 in.		. 11	1. Backfill material (	below filter pack): None Other	
N. I.D. well casing $2.07$ in.				Other	
I hereby certify that the information on this for	m is true and correct to the best	of my knowledge		Date Modified: 7/9/2024	
Signature	Firm Rambo			Tel: (414) 837-	-3607
Ehr			or, Milwaukee, WI 5		